



**COMSOL
CONFERENCE**
ROTTERDAM2013

**Simulation of Flow, Thermal and Mechanical Effects
in COMSOL for Enhanced Geothermal Systems**

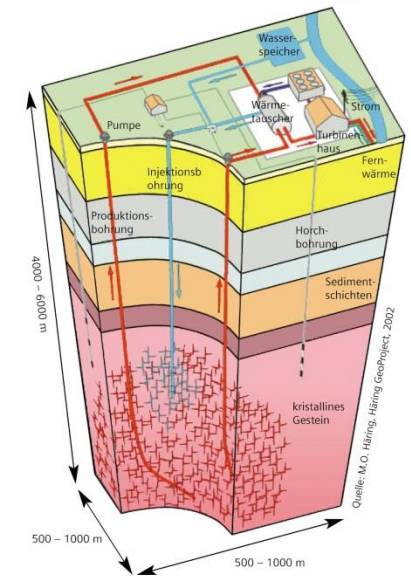
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TNO / Geological Survey of The Netherlands



Enhanced Geothermal Systems

- › Enhanced Geothermal Systems: technology where a hot ($>100^\circ$) but relatively impermeable ($\kappa < 10^{-16} \text{ m}^2$) rock at depth (often $> 2\text{-}3 \text{ km}$) is hydraulically stimulated.
- › Shear failure on **pre-existing** fracture network, giving increased permeability; enabling flow between wells to exchange heat
- › Mechanisms of shear failure (Majer et al., 2007)
 - › Pore pressure \uparrow Effective normal stress \downarrow
 - › Temperature \downarrow Effective normal stress \downarrow
 - › Chemical reaction may reduce coefficient of friction

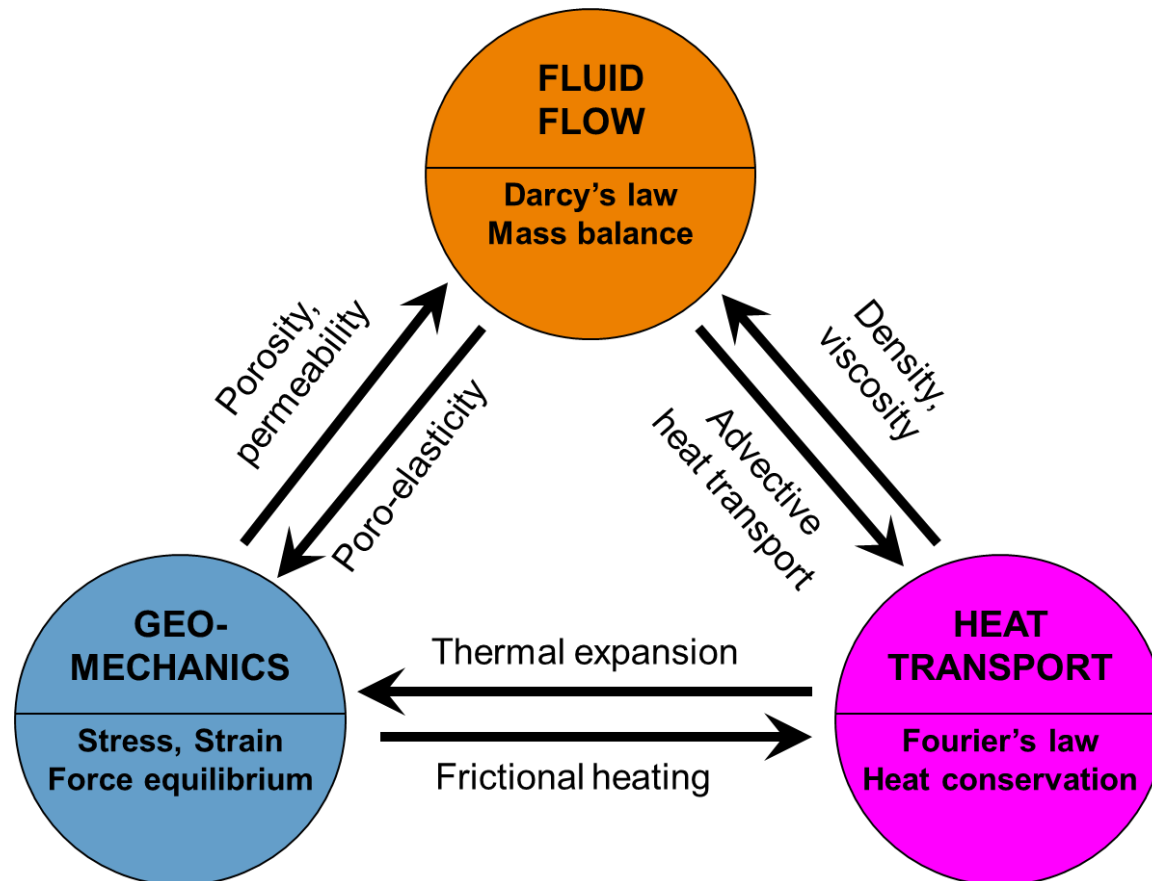


Mohr-Coulomb

$$\tau = S_0 + \mu(\sigma_n - p_f)$$



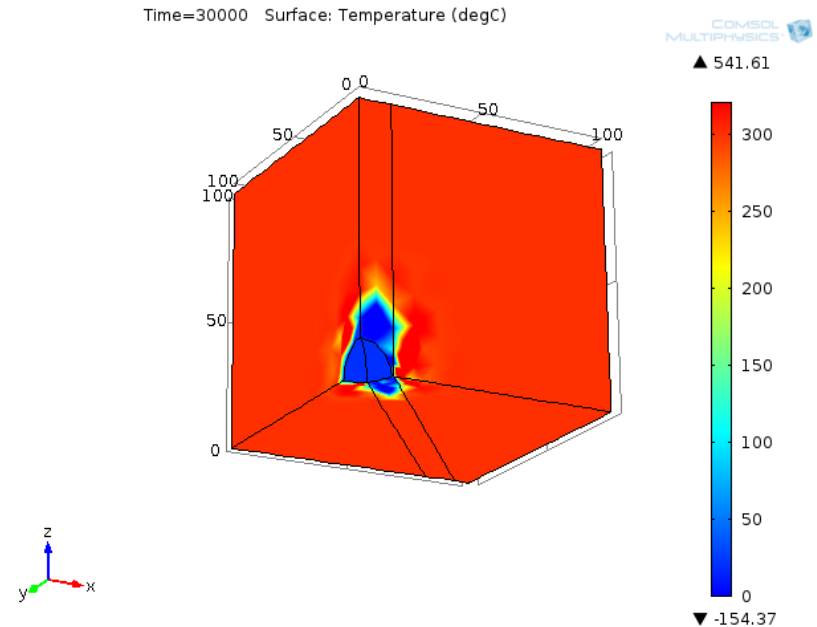
Full Coupling of Flow, Mechanics and Heat Transport





The Model

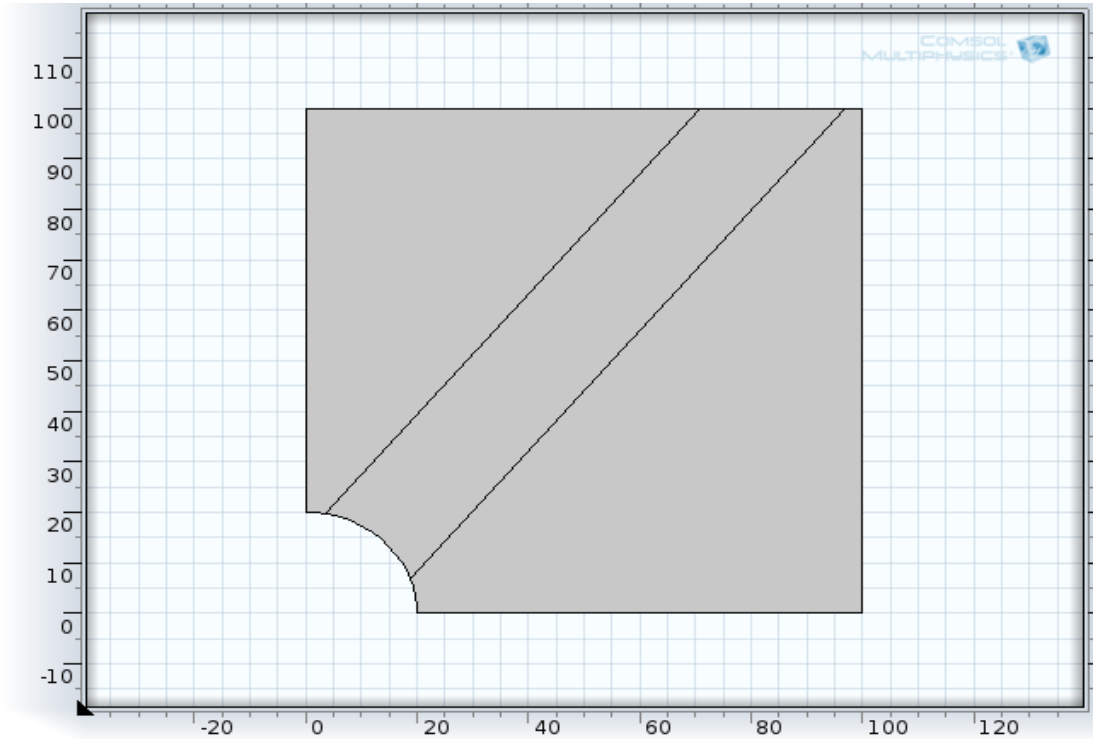
- Inspired by field case (Soult-sous-Forêts)
- 3D rock mass of 100x100x100 m³
- Fracture zone with dip of 60°
- Impermeable matrix of granite
- Fracture zone
 - 20 m thickness
 - Initial permeability of 500 mD
- Vertical injection well
- Injection of cold water (20°C)





2D Model

Sensitivities using
2D cross section





Coupled Processes and COMSOL Multiphysics

- › **Flow** in porous medium
 - › Darcy's law
 - › Continuum equation
 - › Fracture Permeability according to the cubic law (Poisseeuille flow)
 - › Porosity change due to volumetric strain
 - › Viscosity change due to temperature
- › **Mechanics**
 - › Rock matrix: Linear Elastic
 - › Fracture zone: Mohr-Coulomb Model
 - › Poro-elastic stresses
 - › Thermo-elastic stresses
- › **Heat Transfer**
 - › Conduction & Diffusion: Heat equation
 - › Convection: Darcy velocity field



▼ Equation

Show equation assuming:

Study Poro-elastic, Time Dependent

$$-\nabla \cdot \boldsymbol{\sigma} = \mathbf{F}_V, \quad \boldsymbol{\sigma} = \mathbf{s}$$

$$\mathbf{s} - \mathbf{s}_0 = \underline{\underline{\mathbf{C}}} : (\boldsymbol{\epsilon} - \boldsymbol{\epsilon}_0 - \boldsymbol{\epsilon}_{inel}) - (\text{trace}(\underline{\underline{\mathbf{C}}} : (\boldsymbol{\epsilon} - \boldsymbol{\epsilon}_0 - \boldsymbol{\epsilon}_{inel}))/3 + p_w) \mathbf{I} \quad \alpha_B pf \mathbf{I}$$

$$\boldsymbol{\epsilon} = \frac{1}{2} [(\nabla \mathbf{u})^T + \nabla \mathbf{u}]$$

Modelled as initial stress

$$\rho S \frac{\partial pf}{\partial t} + \nabla \cdot (\rho \mathbf{u}) = Q_m - \rho \alpha_B \frac{\partial e_{vol}}{\partial t}$$

$$\mathbf{u} = -\frac{\kappa}{\mu} \nabla pf$$

Has to be modelled in Darcy Law as a source term

$$S = \epsilon_p \chi_f + \frac{(\alpha_B - \epsilon_p)(1 - \alpha_B)}{\kappa}$$

► Model Inputs

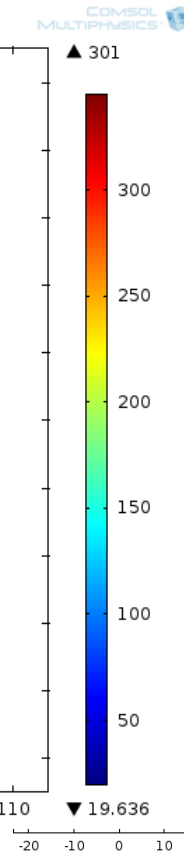
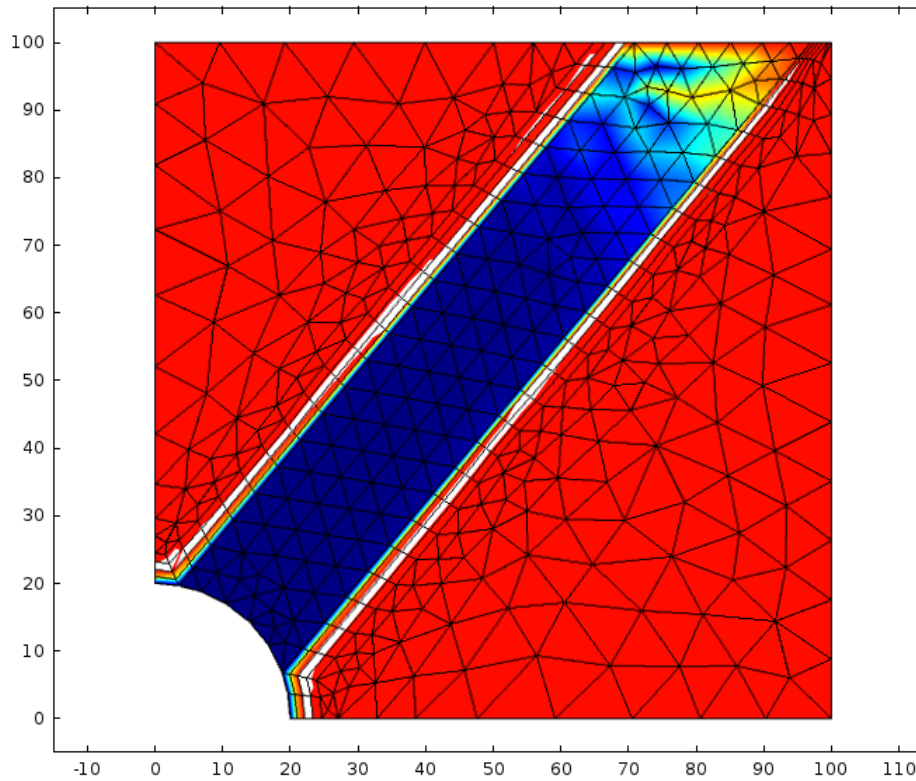
storage has to be calculated



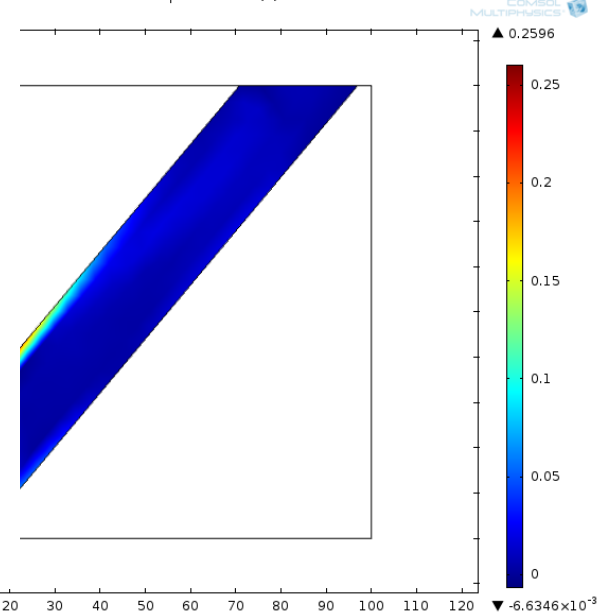


Sensitivity to meshing

Time=2.372932e5 Surface: Temperature (degC) Mesh



e5 Surface: Effective plastic strain (1)



Temperature case 1 after 55 hours of injection.

- $T_{matrix} = 300^{\circ}C$
- $T_{fluid} = 20^{\circ}C$

Effective plastic strain

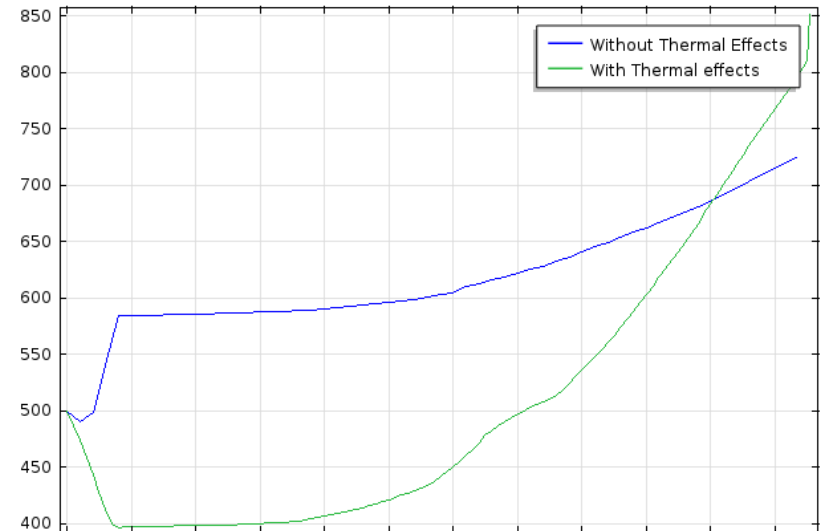


Thermal Effects

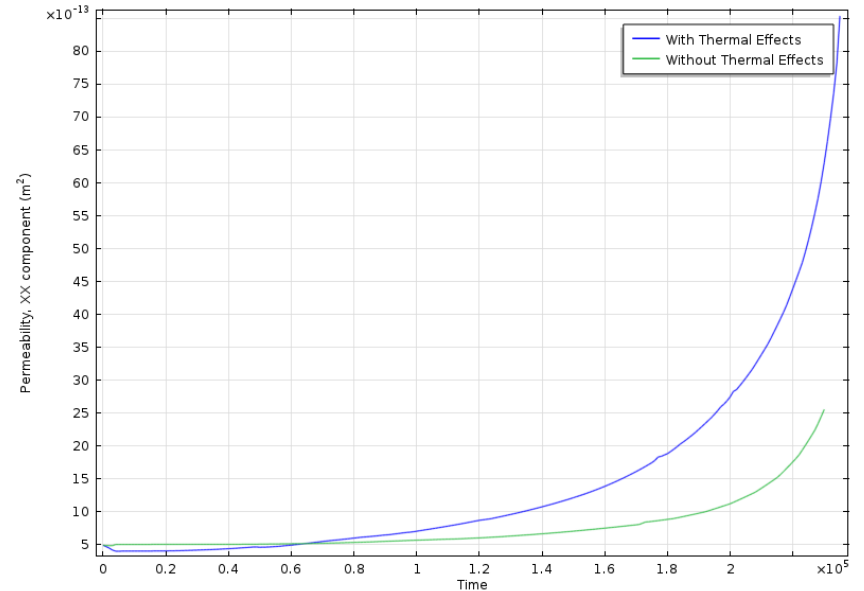
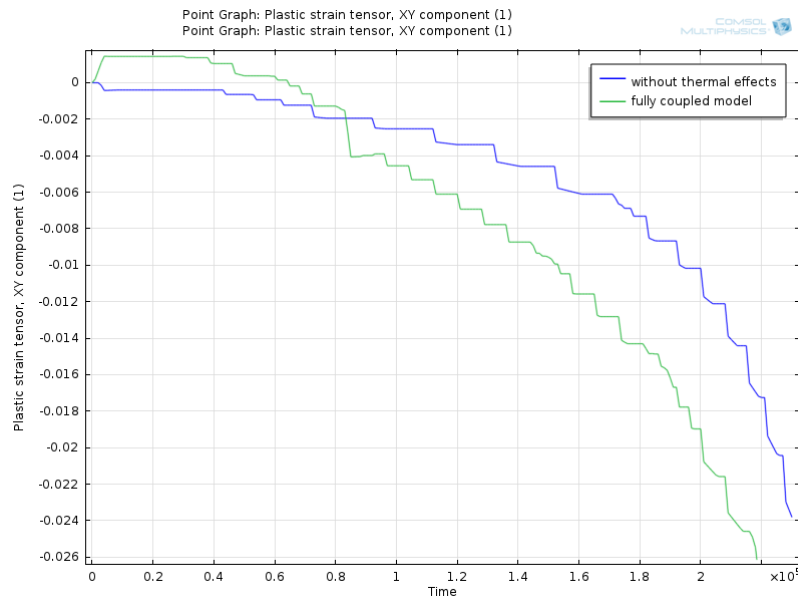
Neglecting thermal effects is not justified

- different behaviour of permeability
- shear strain changes sign

Point Graph: Case 2A (mD) Point Graph: Permeability, XX component (mD)



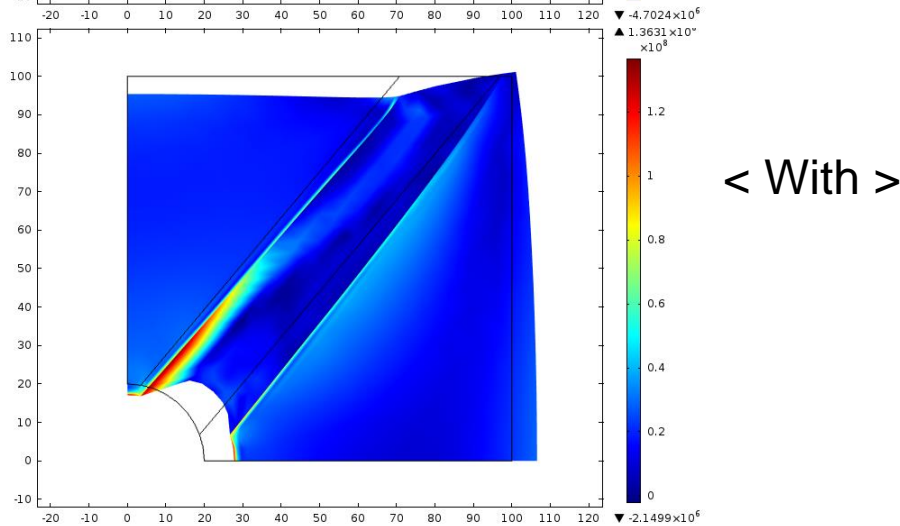
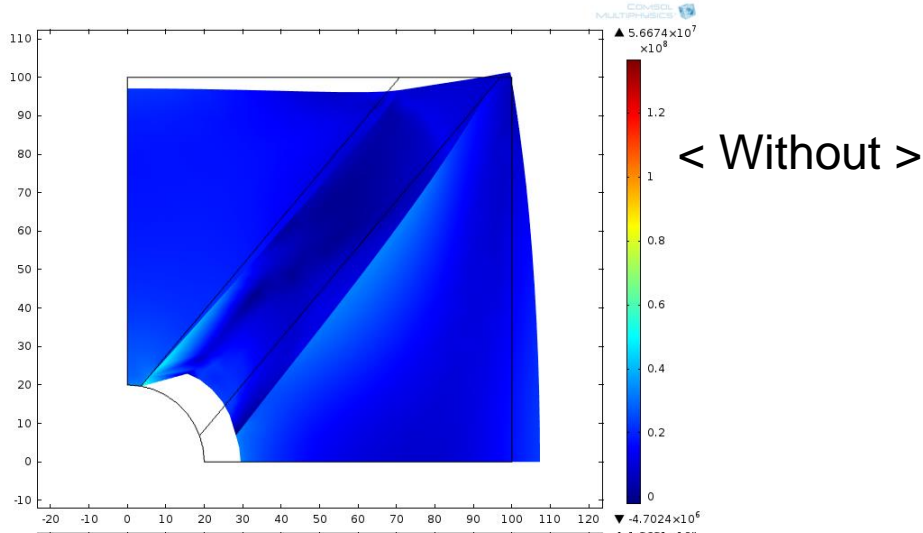
Point Graph: Permeability,t (m²)



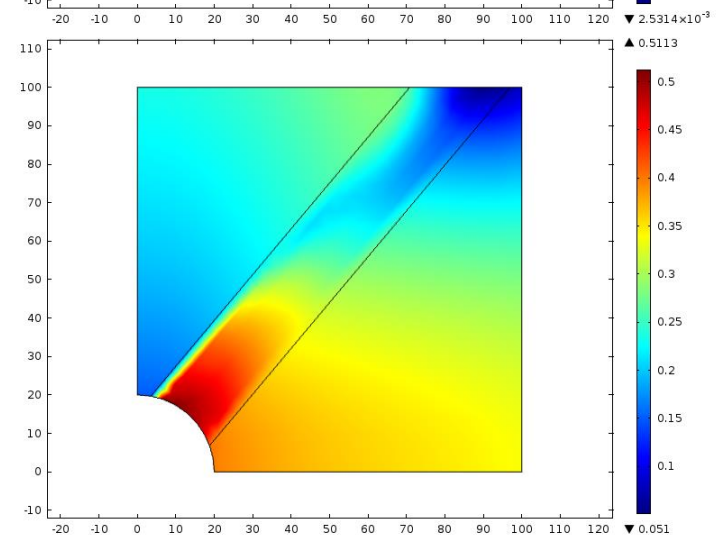
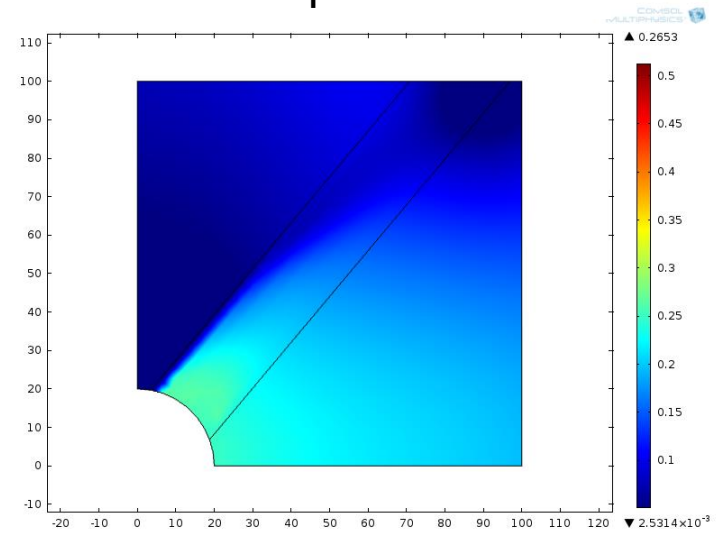


Thermal Effects

Von Mises stress



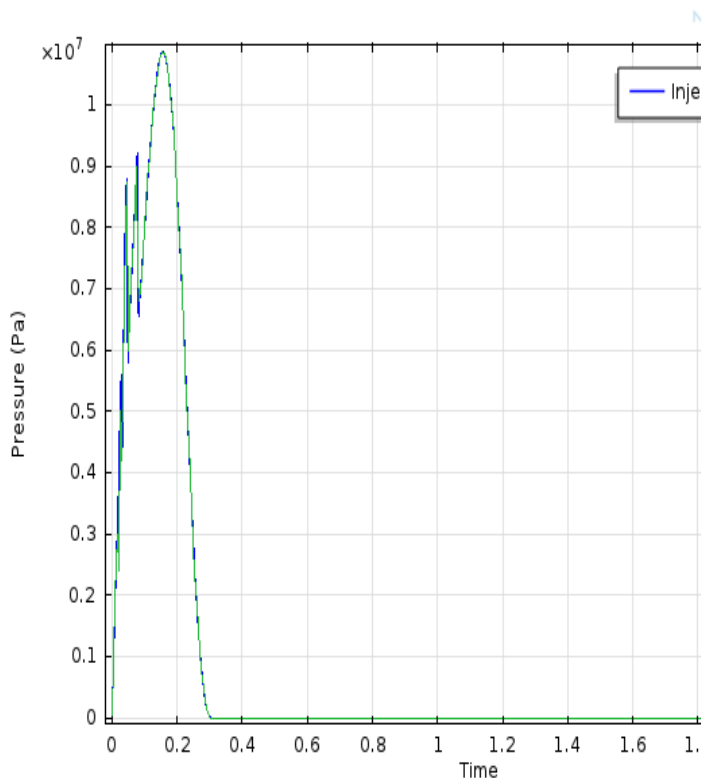
Total Displacement





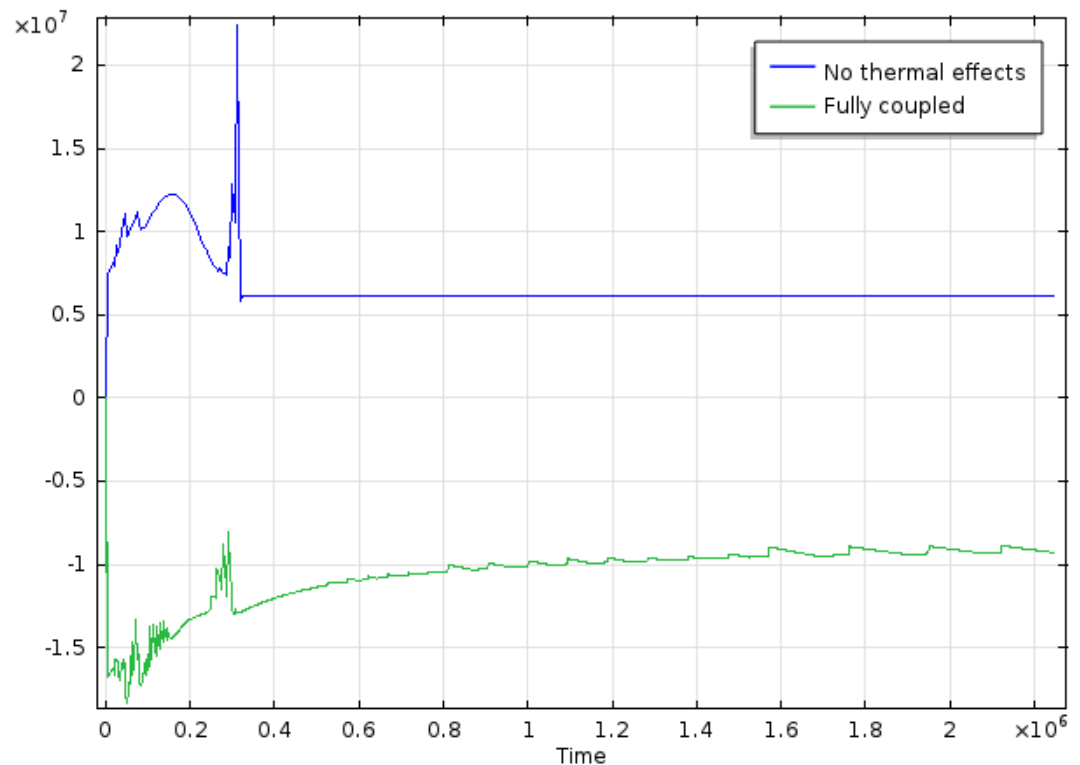
Effect of stopping injection

- ▶ Well pressure (actual injection scheme)



- ▶ Pressure in solid
 - ▶ Cooling reduces pressure
 - ▶ Continued effect

Point Graph - point 4: Pressure (Pa) in solid





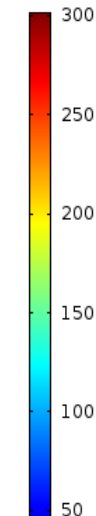
Temperature effects after shutdown

Temperature

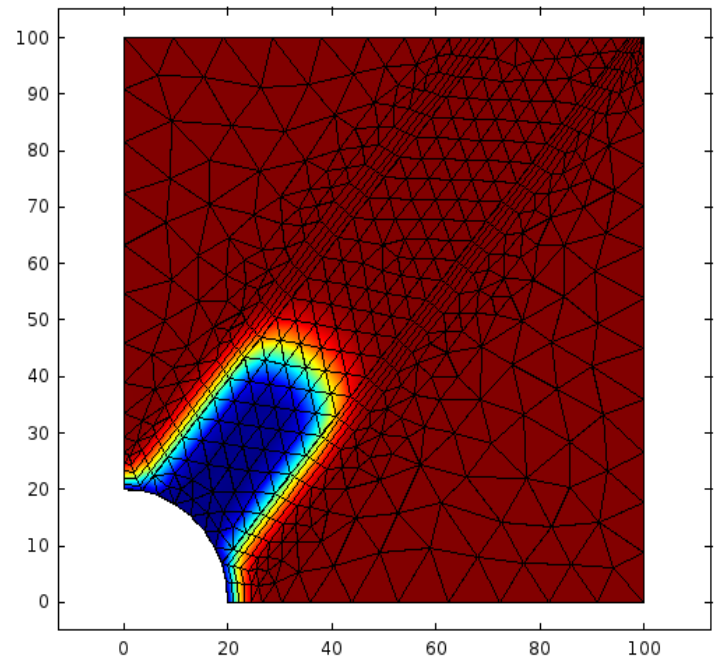
Time=2.25e6 Surface: Temperature (degC) Mesh

COMSOL
MULTIPHYSICS

▲ 300.58



▼ 17.03



Von Mises stress

Time=2.25e6 Surface: von Mises stress, Gauss-point evaluation (Pa)

COMSOL
MULTIPHYSICS

▲ 1.6909x10⁷

x10⁷

3.5

3

2.5

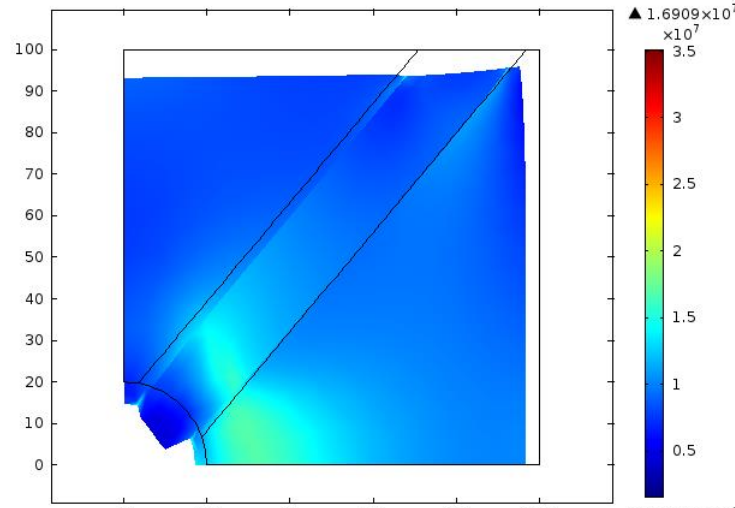
2

1.5

1

0.5

0



No TE effects

With TE effects

▲ 4.7886x10⁶

x10⁷

3.5

3

2.5

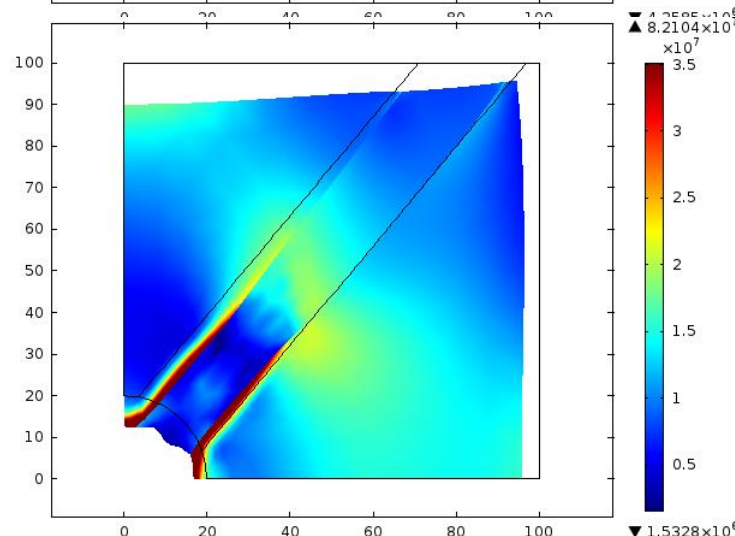
2

1.5

1

0.5

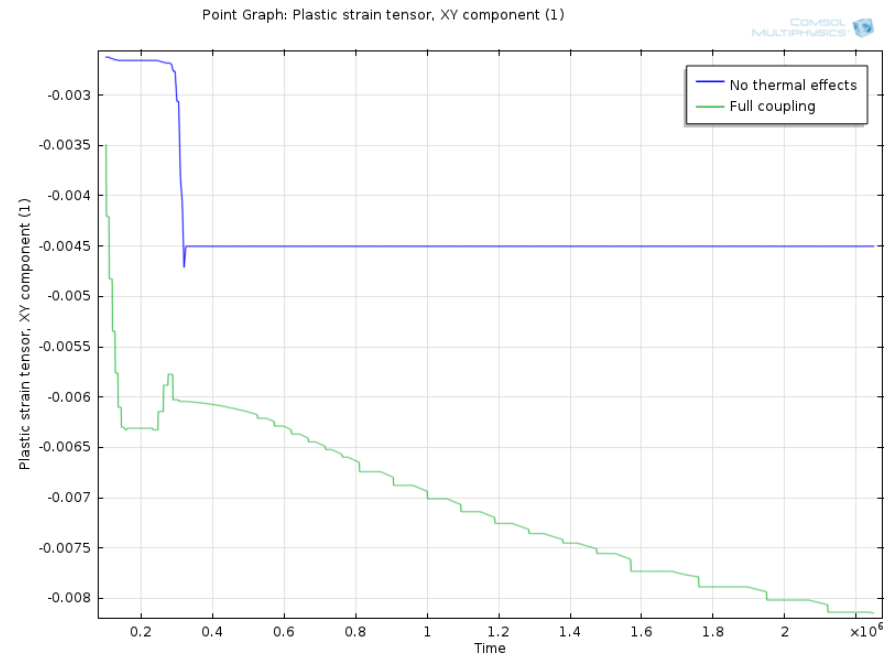
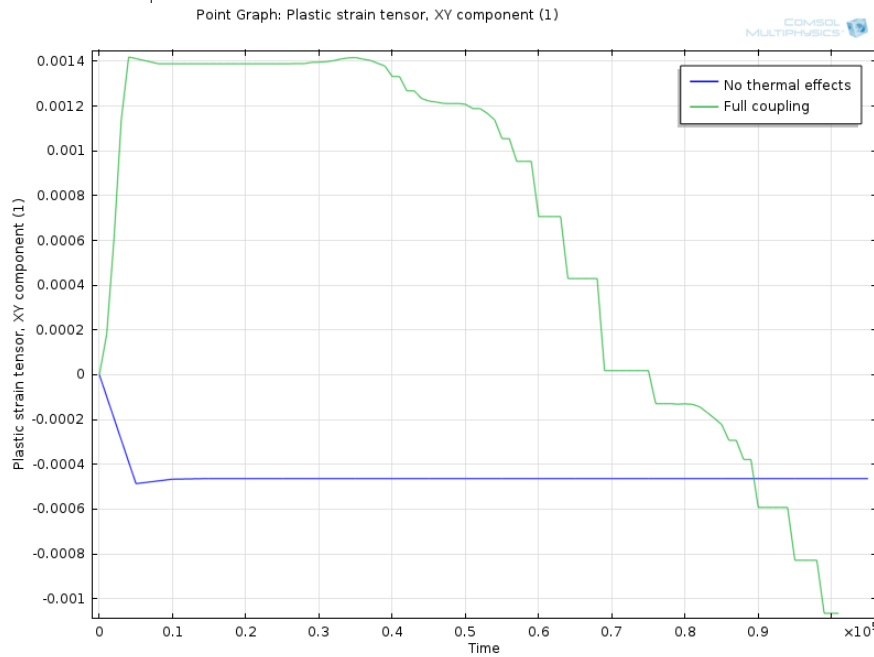
0



▼ 1.5328x10⁶



Plastic Strain: Evolution during injection time and after shutin





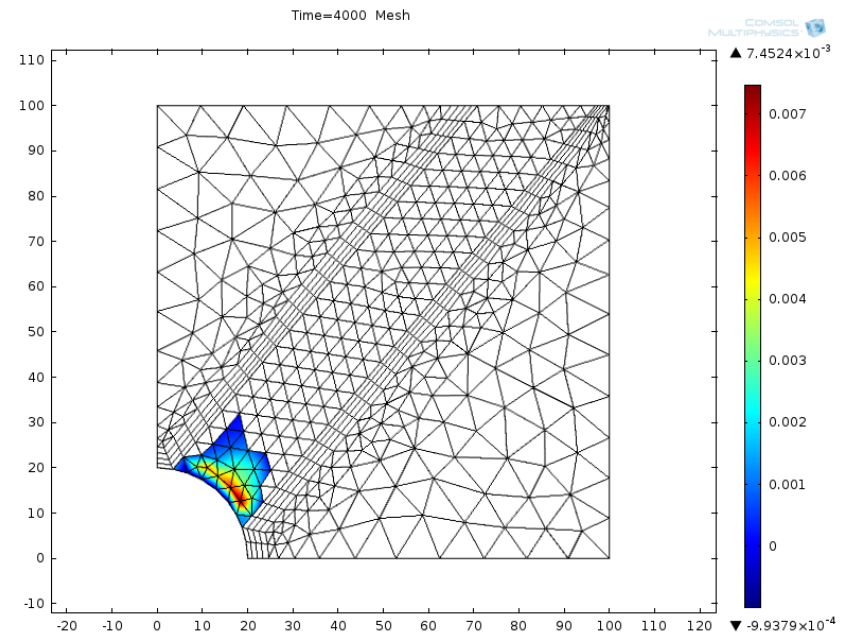
Induced seismicity

- › $M = G d A$
- › Shear displacement = shear strain * H
- › Failing area: 3rd dimension is missing – estimation of H=10 or 20m

Effective plastic strain > 0

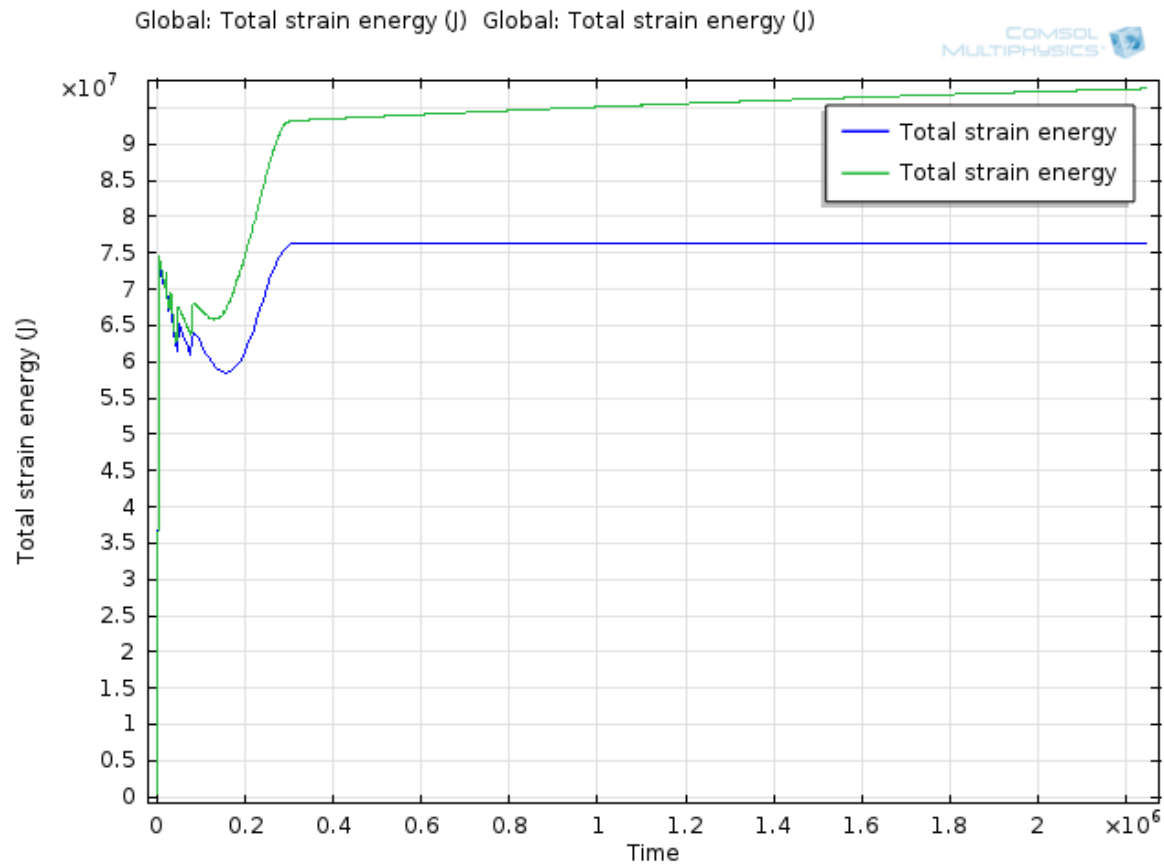
Failing patch

Shear strain





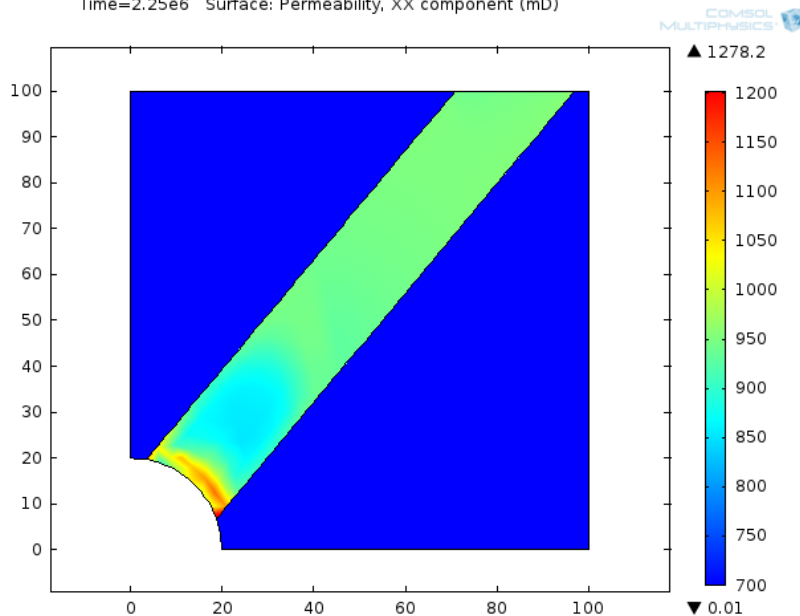
Strain Energy



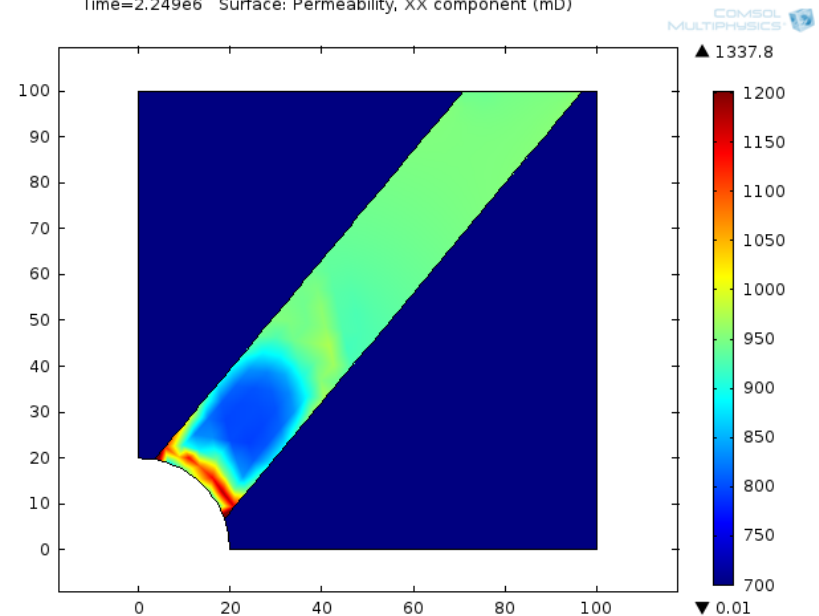


Injection of warmer water vs. injection of cold water – comparison with a field case (Iceland)

Time=2.25e6 Surface: Permeability, XX component (mD)



Time=2.249e6 Surface: Permeability, XX component (mD)



Injectivity_cold/ Injectivity_warm=1.45 Modeling
result

Injectivity_cold/ Injectivity_warm=5.85 at well NH-09

Injectivity_cold/ Injectivity_warm=3.3 at well NH-12

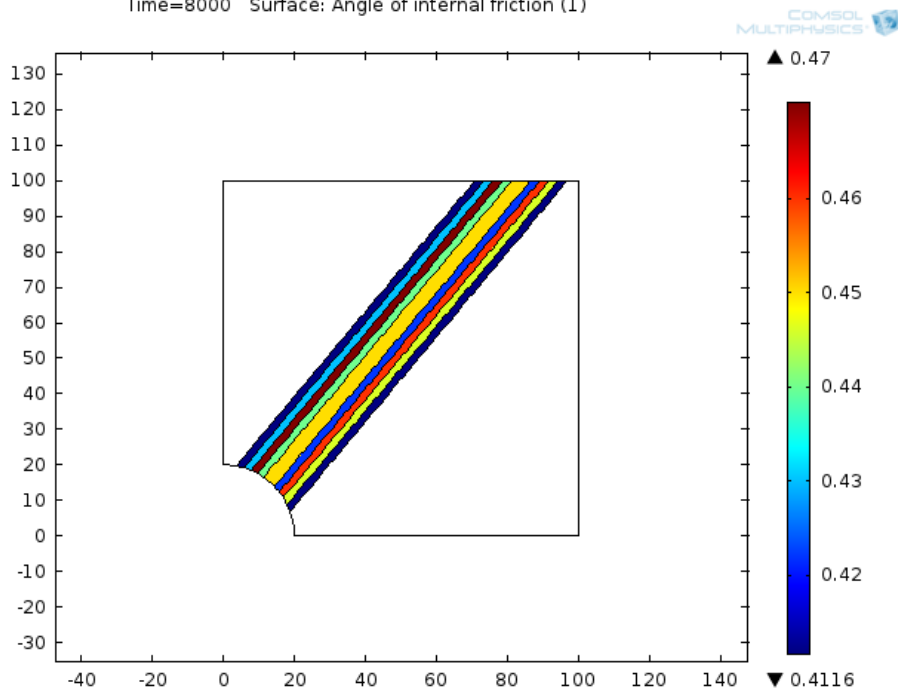
In Iceland geothermal field



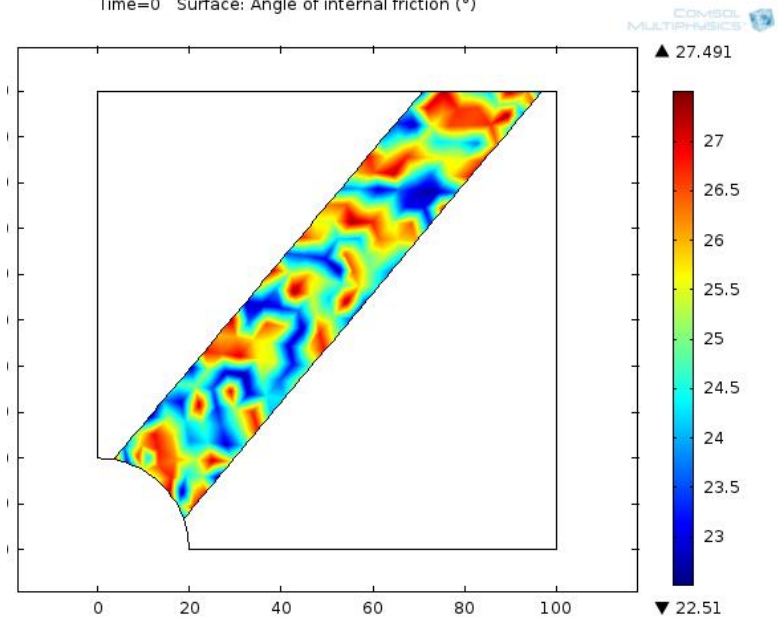
Uncertain parameter: friction angle in Mohr-Coulomb shear failure

Uniform vs. 9 domains vs. random

Time=8000 Surface: Angle of internal friction (1)



Time=0 Surface: Angle of internal friction (*)





Conclusion & Discussion

- › COMSOL is suitable as tool for sensitivity analysis – strong in coupled modelling; issues remain with stability for 3D models
- › Thermal stresses **can instantly change permeability and plastic strain**, changing injectivity and induced seismicity potential
- › Qualitative but not yet quantitative agreement of temperature effect on injectivity for Iceland geothermal field
- › Identified factors relevant for the induced seismicity – calibration still required



Future Work

- › Shear weakening
- › Healing
- › Heterogeneity
- › Influence of geometry on injectivity and seismicity
- › Probabilistic modelling with a proxy model