

Simulation and numerical implementation of chemo-thermomechanical aging of rubber

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Outline

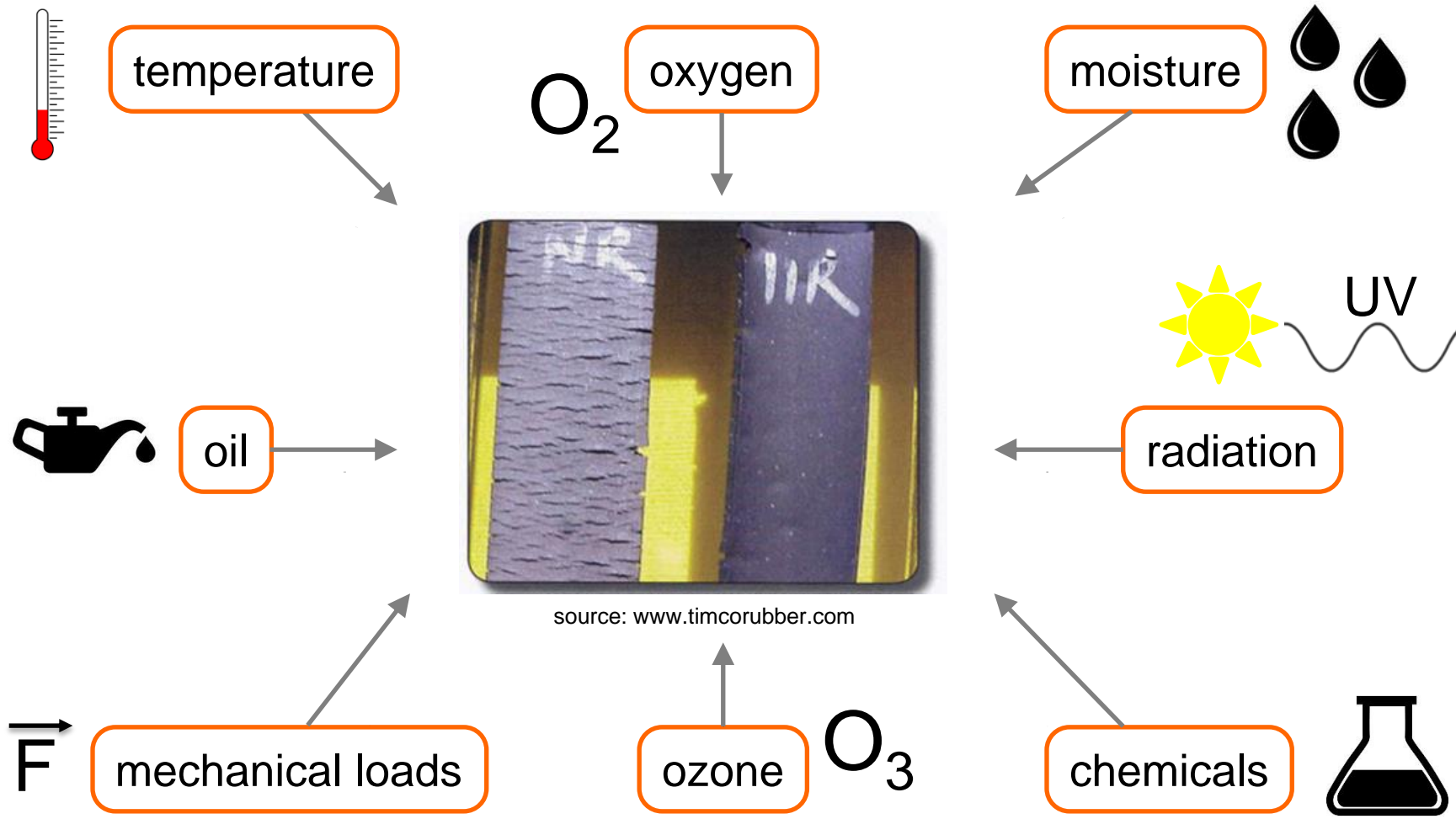
- Introduction and motivation
- Constitutive modelling approach
- Implementation into COMSOL
- Simulations
- Summary and outlook

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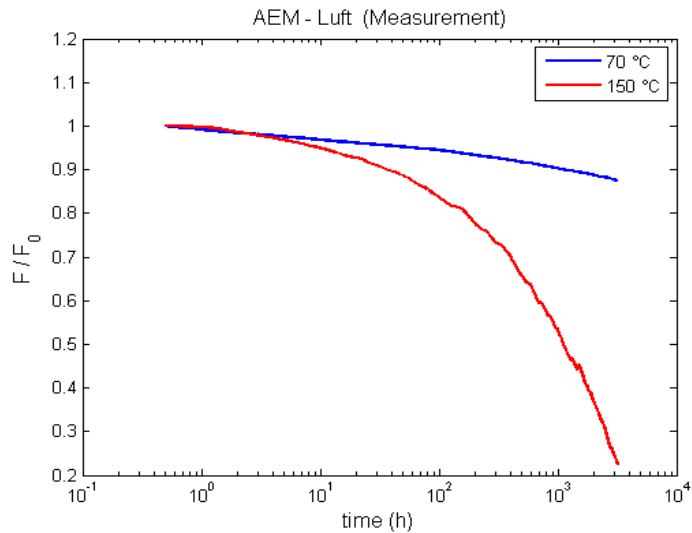
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Introduction & motivation

External influences on elastomers in technical applications



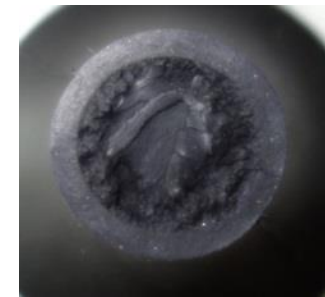
Introduction & motivation



Aging induced stress relaxation



Tension/Compression set

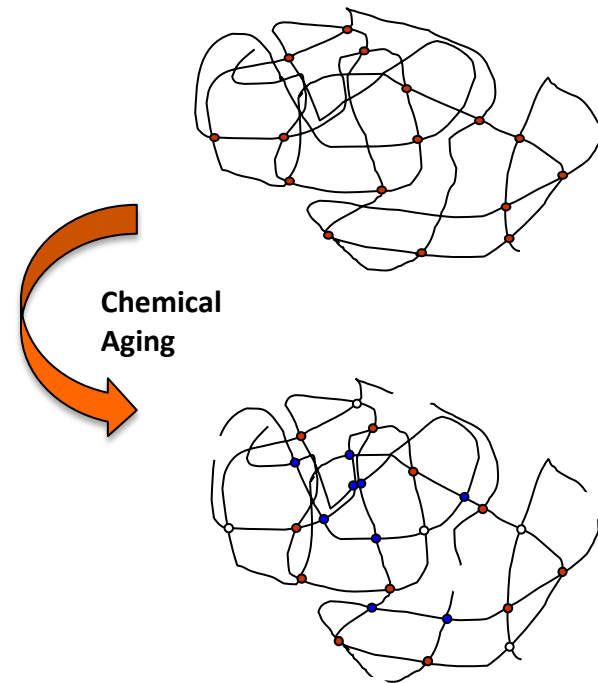
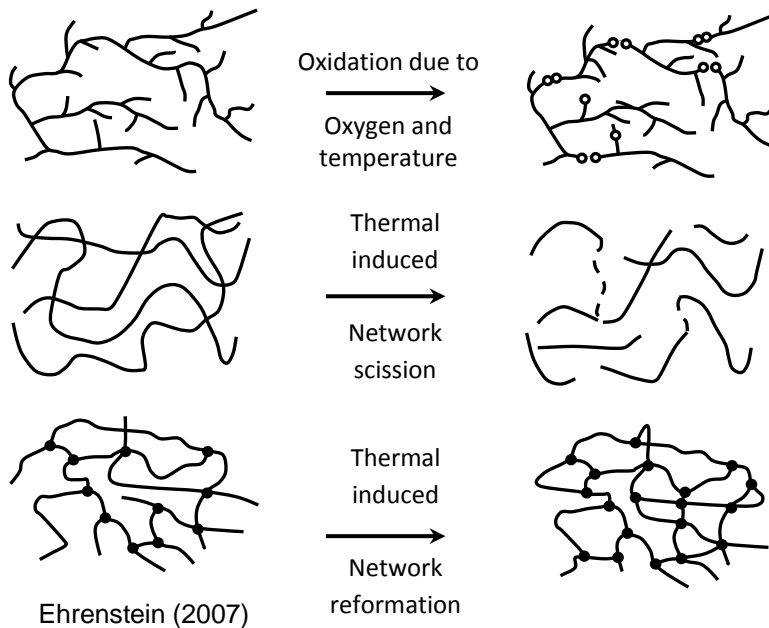


DLO Effect

Modell requirements

- Change of mechanical properties due to aging
- Tension/Compression set
- DLO Effect
- Material behavior: nonlinear thermoviscoelasticity

Introduction & motivation



Chemical Aging

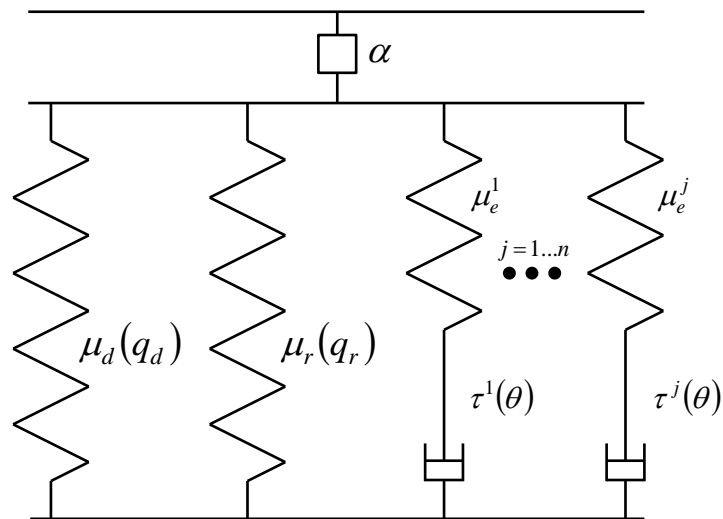
- Irreversible chemical change as a result of oxygen diffusion and reaction with the elastomer; elevated temperatures accelerate the aging process
- Degeneration of chemical bonds (**Network-Degradation**)
- Formation of new network junctions (**Network-Reformation**)

Outline

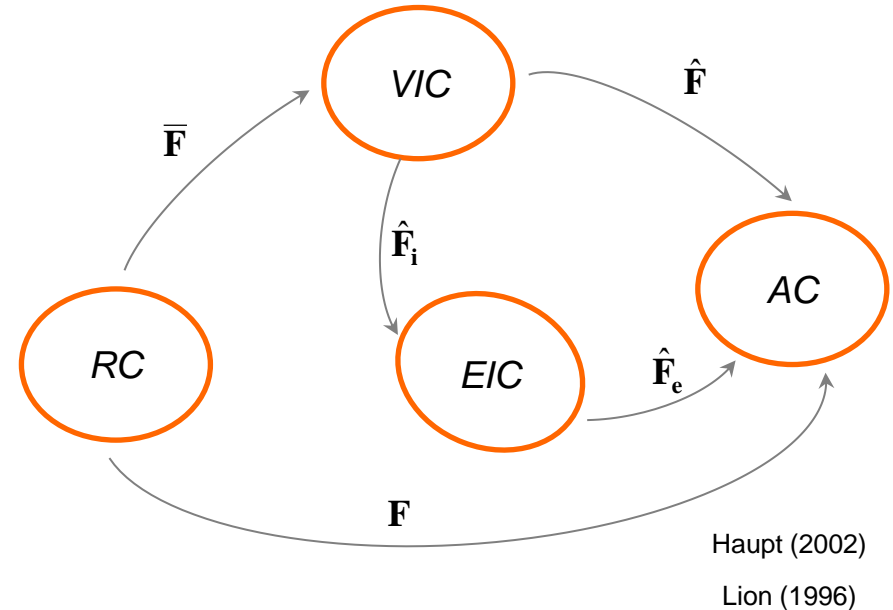
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Modelling

- Rheological model
(Neo-Hooke)



- General motion of a deformable body



- Thermo-mechanical consistence (C.-D. inequality)

$$-\rho_0 \dot{\psi} + \tilde{\mathbf{T}} : \dot{\mathbf{E}} - \rho_0 s \dot{\theta} - \frac{\mathbf{q}}{\theta} \cdot \text{Grad} \theta \geq 0$$

$$\psi = \psi(\hat{\mathbf{C}}, \hat{\mathbf{C}}_e, J, \theta, q_d, q_r, c) \longrightarrow \text{Helmholz free energy function}$$

Modelling

Set of constitutive eq. and evolution eq. can be evaluated

- Stress (2.PK)

$$\tilde{\mathbf{T}} = \tilde{\mathbf{T}}_{eq}^{VOL} + \tilde{\mathbf{T}}_d^{ISO} + \tilde{\mathbf{T}}_r^{ISO} + \tilde{\mathbf{T}}_{neq}^{ISO}$$

$$\tilde{\mathbf{T}} = K[(J-1) + \ln J/J]J\mathbf{C}^{-1} - K\alpha(\theta - \theta_0)J\mathbf{C}^{-1} + \mu_d(q_d)J^{-2/3}\left(\mathbf{1} - \frac{1}{3}\text{tr}(\hat{\mathbf{C}})\hat{\mathbf{C}}^{-1}\right) + J^{-2/3}\left(\hat{\mathbf{T}}_r - \frac{1}{3}(\hat{\mathbf{T}}_r : \hat{\mathbf{C}})\hat{\mathbf{C}}^{-1}\right) + \mu_e J^{-2/3}\left(\hat{\mathbf{C}}_i^{-1} - \frac{1}{3}\text{tr}(\hat{\mathbf{C}}_i^{-1}\hat{\mathbf{C}})\hat{\mathbf{C}}^{-1}\right)$$

- Evolution equations

$$\dot{\hat{\mathbf{T}}}_r = q_r(t) \hat{\mathbf{C}}(t) : \dot{\hat{\mathbf{C}}}$$

→ Evolution eq. for the stress of the newly reformed network

$$\dot{\hat{\mathbf{C}}}_i^j = 2\left(\mathbf{C} - \frac{1}{3}\text{tr}(\mathbf{C}(\hat{\mathbf{C}}_i^j)^{-1})\hat{\mathbf{C}}_i^j\right) / \tau^j(\theta)$$

→ Evolution eq. for inelastic deformation

$$\dot{q}_d = \frac{1}{j} \sum_j c v_d^j \exp\left(\frac{-E_d^j}{R\theta}\right) (1 - q_d^j)$$

$$\dot{q}_r = \frac{1}{j} \sum_j c v_r^j \exp\left(\frac{-E_r^j}{R\theta}\right) (1 - q_r^j)$$

→ Evolution eq. for the internal (aging) variables q_d and q_r Jöhrlitz (2012)

Modelling

Set of constitutive eq. and evolution eq. can be evaluated

- Heat flux, diffusion flux, reaction term

$$\mathbf{q} = -\lambda_{\theta} \text{ Grad} \theta - \lambda_c (\zeta \delta^2 + \zeta \delta \theta) c \text{ Grad} c$$

$$\mathbf{j} = -\lambda_c (\delta + \zeta \theta) \text{ Grad} c$$

$$\hat{c} = -k (\delta c + \zeta c \theta)$$

Johlitz (2012)

$$\xrightarrow{\delta = 1 \quad \zeta = 0}$$

$$\mathbf{q} = -\lambda_{\theta} \text{ grad} \theta \quad (\text{Fourier's law})$$

$$\mathbf{j} = -\lambda_c \text{ grad} c \quad (\text{Fick's law})$$

$$\hat{c} = -k c \quad (\text{linear reaction})$$

- Temperature and aging dependency of diffusion and reaction coefficient Johlitz (2012)

$$\lambda_c = \lambda_{c_0} \exp\left(-\frac{E_c}{R\theta}\right) \exp(-\gamma q_r)$$

$$k = [k_{01}(1 - q_d) + k_{02}(1 - q_r)] \exp\left(-\frac{E_k}{R\theta}\right)$$

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Implementation

Weak formulation of the problem

$$0 = \int_{\Omega} \text{weak } \delta V$$

- Balance momentum equation

$$0 = - \int_V \delta \mathbf{E}(\mathbf{u}) : \tilde{\mathbf{T}}(\boldsymbol{\theta}, \mathbf{c}, \mathbf{q}_d(\mathbf{c}), \mathbf{q}_r(\mathbf{c})) dV - \int_V \delta \mathbf{u} \mathbf{b} dV + \int_S \delta \mathbf{u} \mathbf{t} dS$$

- Heat conduction equation

$$0 = - \int_V \delta \theta \rho c_p \dot{\theta} dV - \int_V \text{Grad}(\delta \theta) [\lambda_{\theta} \text{Grad} \theta + \lambda_c [\zeta \delta^2 + \zeta \delta \theta] \mathbf{c} \text{Grad} \mathbf{c}] dV - \int_S \delta \theta q^* dS$$

- Diffusion-Reaction equation

$$0 = - \int_V \delta \mathbf{c} [\rho \dot{\mathbf{c}} + k[\mathbf{c} \delta + \zeta \mathbf{c} \boldsymbol{\theta}]] dV - \int_V \text{Grad}(\delta \mathbf{c}) \lambda_c (\delta + \zeta \boldsymbol{\theta}) \text{Grad} \mathbf{c} dV - \int_S \delta \mathbf{c} \mathbf{j}^* dS$$

→ Strongly coupled multifield problem

Implementation

Weak form eq.

Evolution eq.

Model Builder

- Component 1 (comp1)
 - Definitions
 - a= Aging
 - a= NO Aging
 - a= F
 - a= FT
 - a= C
 - a= Cinv
 - a= C_iso
 - a= Ic / Ic_iso
 - a= Cinv_iso
 - a= E
 - a= J
 - a= Volu_mech/therm
 - a= S_hyper
 - a= S_hyper_Vollso
 - a= Ci_inv1
 - a= Ci_inv2
 - a= Ci_inv3
 - a= Ci_inv4
 - a= Sneq1
 - a= Sneq2
 - a= Sneq3
 - a= Sneq1_Vollso
 - a= Sneq2_Vollso
 - a= Sneq3_Vollso
 - a= Sneq4_Vollso
 - a= Seq
 - a= Seq_Vollso
 - a= Seq_d
 - a= Seq_d_Vollso
 - a= Seq_ges
 - a= Seq_ges (hypoelast3)
 - a= S_visko 1M
 - a= S_visko 2M
 - a= S_visko 3M
 - a= S_visko 4M
 - a= S_ohneVisko
 - a= P
 - a= T
 - a= hypoelast2
 - a= hypoelast3 (dSr) NeoHooke
 - a= Chem (k)
 - a= qd / qr
 - a= Heat (Cp)

- Created tensor library:
 - Basic tensors
 - Constitutive laws
 - Auxiliary variables

Name	Expression
S11	S11eq+S11neq_1+S11neq_2+S11neq_3+S11neq_4
S12	S12eq+S12neq_1+S12neq_2+S12neq_3+S12neq_4
S13	S13eq+S13neq_1+S13neq_2+S13neq_3+S13neq_4
S22	S22eq+S22neq_1+S22neq_2+S22neq_3+S22neq_4
S23	S23eq+S23neq_1+S23neq_2+S23neq_3+S23neq_4
S33	S33eq+S33neq_1+S33neq_2+S33neq_3+S33neq_4

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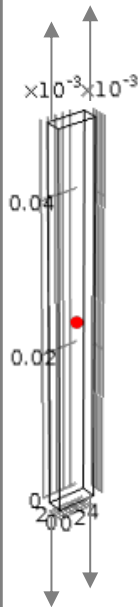
Simulations

- Measured parameters

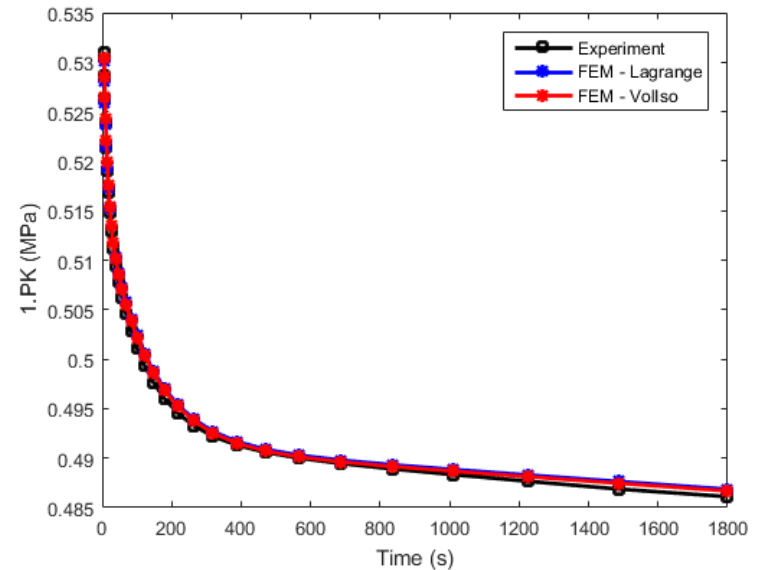
- Material parameters: $\mu_0, \mu_r, \mu_e, \tau(\theta)$
- Aging parameters: E_d, ν_d, E_r, ν_r
- Thermal parameters: $c_p(\theta), \alpha(\theta), \lambda_\theta$

- Estimated parameters

- Chemical parameters: $\lambda_{c_0}, E_c, k_{01}, k_{02}, E_k, \gamma, \delta, \zeta$

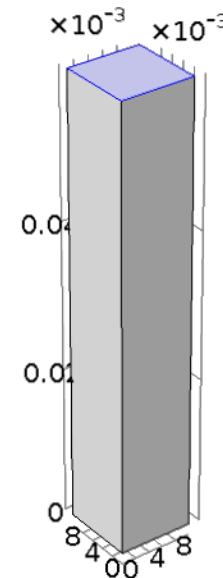
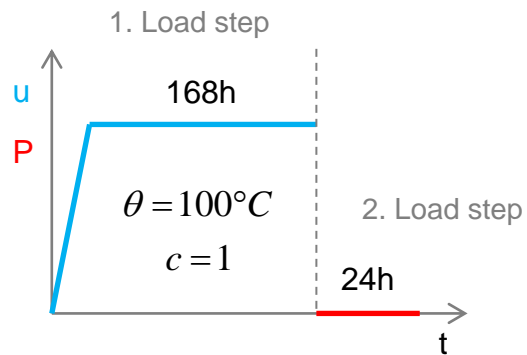


- 3D uniaxial relaxation test in tension
- Model without aging
- Comsol vs. Experiment** (NBR rubber)



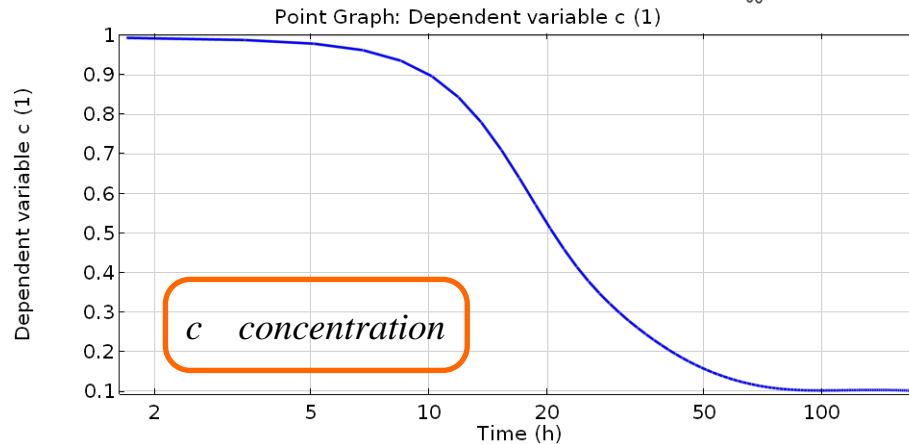
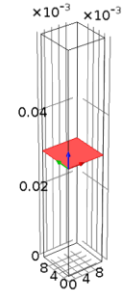
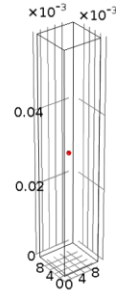
Simulations

- BC:
 - 1. LS – applied displacement u
 - 2. LS – applied zero stress P

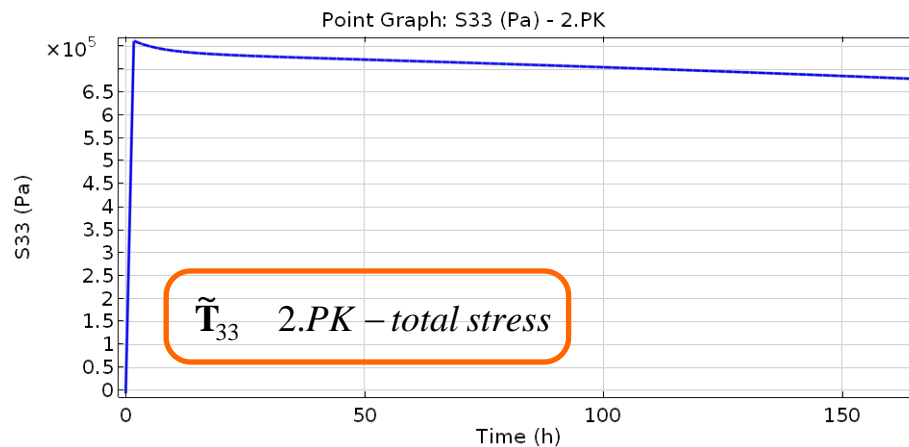
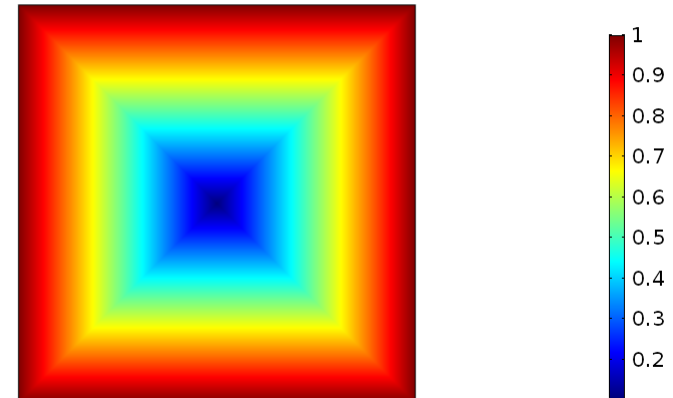


Simulations

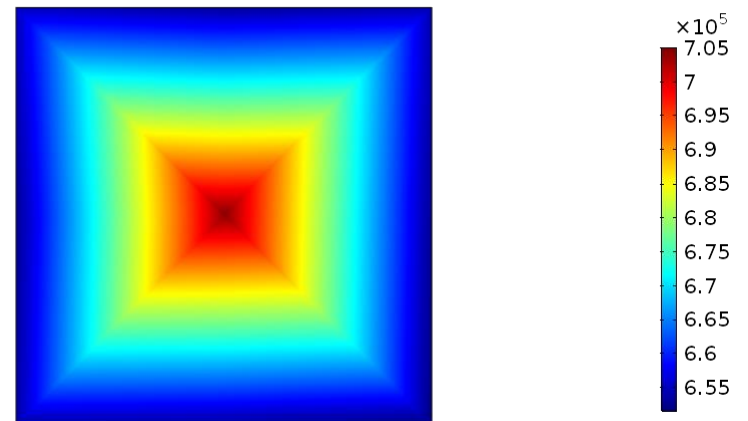
- 1. Load step results



Time=6.0486E5 s Surface: Dependent variable c (1)

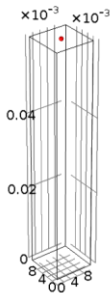


Time=5.9264E5 s Surface: Dependent variable S33(Pa)

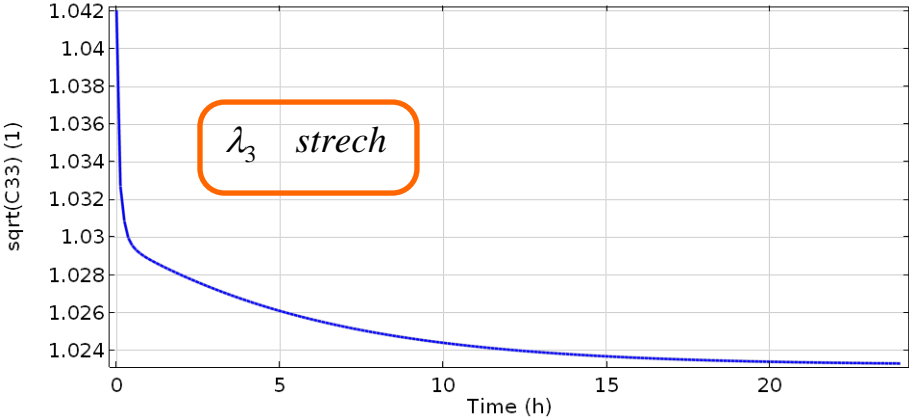


Simulations

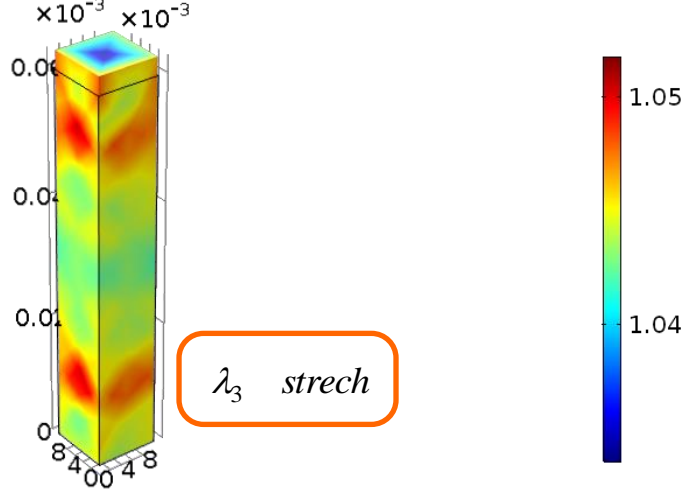
- 2. Load step results



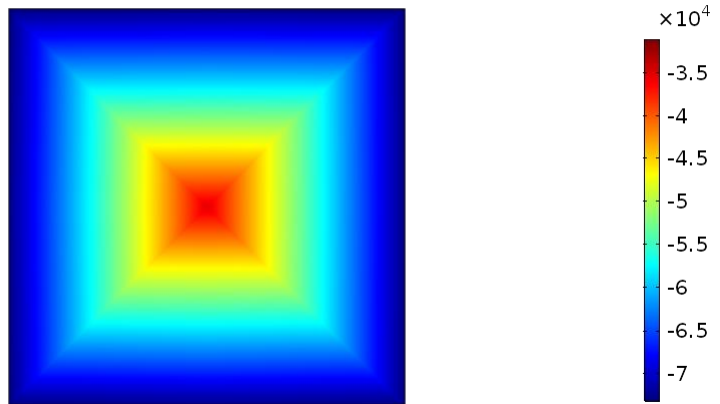
Point Graph: sqrt(C33) (1)



Time=434.17 s Surface: sqrt(C33) (1)



Time=434.17 s Surface: Dependent variable S33eq_r (Pa)



\tilde{T}_{r33} 2.PK – Stress of reformed network

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Summary & outlook

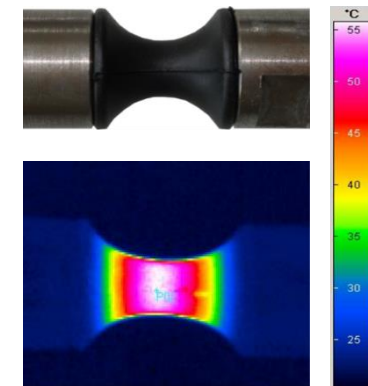
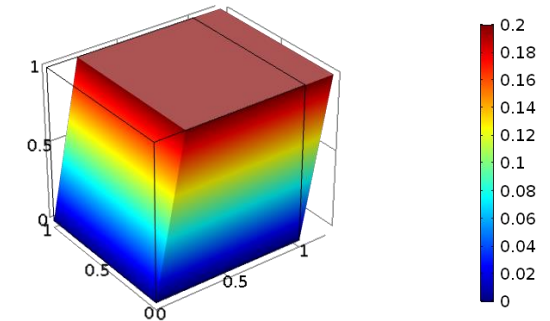
Summary

- Introduction to aging processes
- Model overview – phenomenological approach
- Modeling of aging, tension set and DLO effect
- Modeling of material behavior: nonlinear thermoviscoelasticity

Outlook

- Experimental identification of chemical parameters
- Simulation of an industrial component
- Include aging due to dissipative heating

Time=1800 s Surface: Dependent variable u1 (1)



COMSOL Conference 2016 Munich

Thank you.