



Numerical model for rocking of a mono-pile in a porous seabed

D-S Jeng, X-D Luo and J-S Zhang
Division of Civil Engineering, University of Dundee, UK

18th November 2010

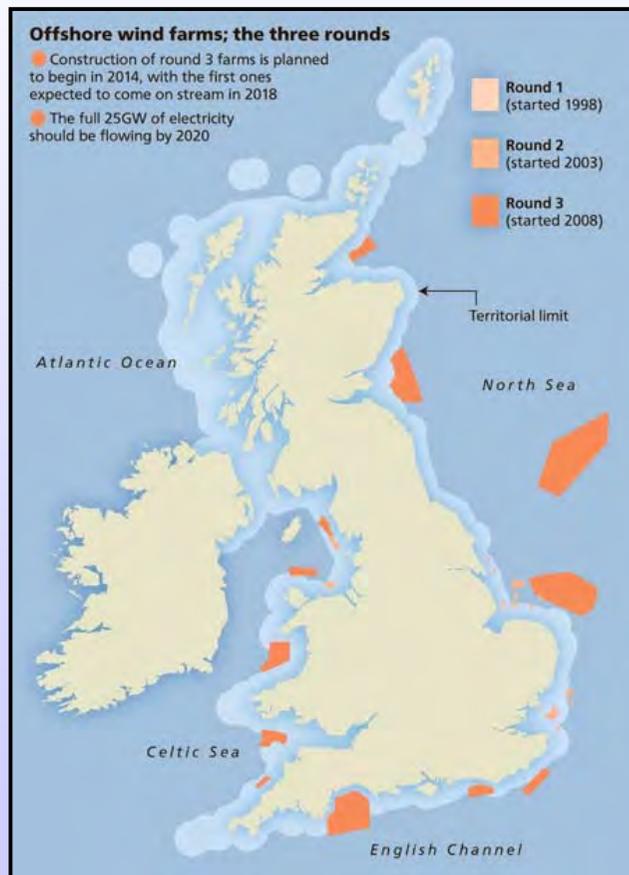


Outline

1. Introduction
2. Theoretical formulations
3. Numerical results
4. Conclusions & future work

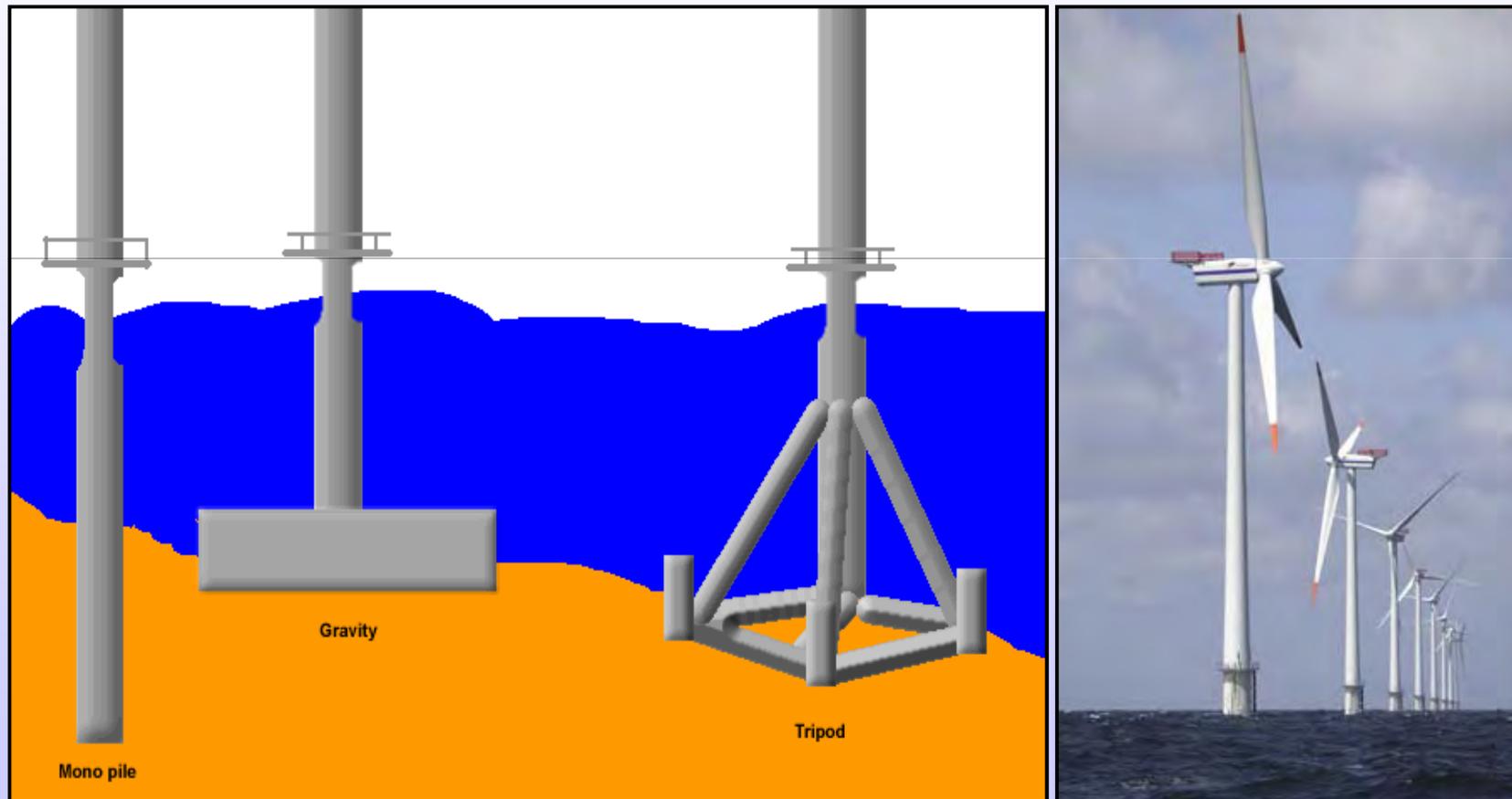
1. Introduction

Offshore windfarm system



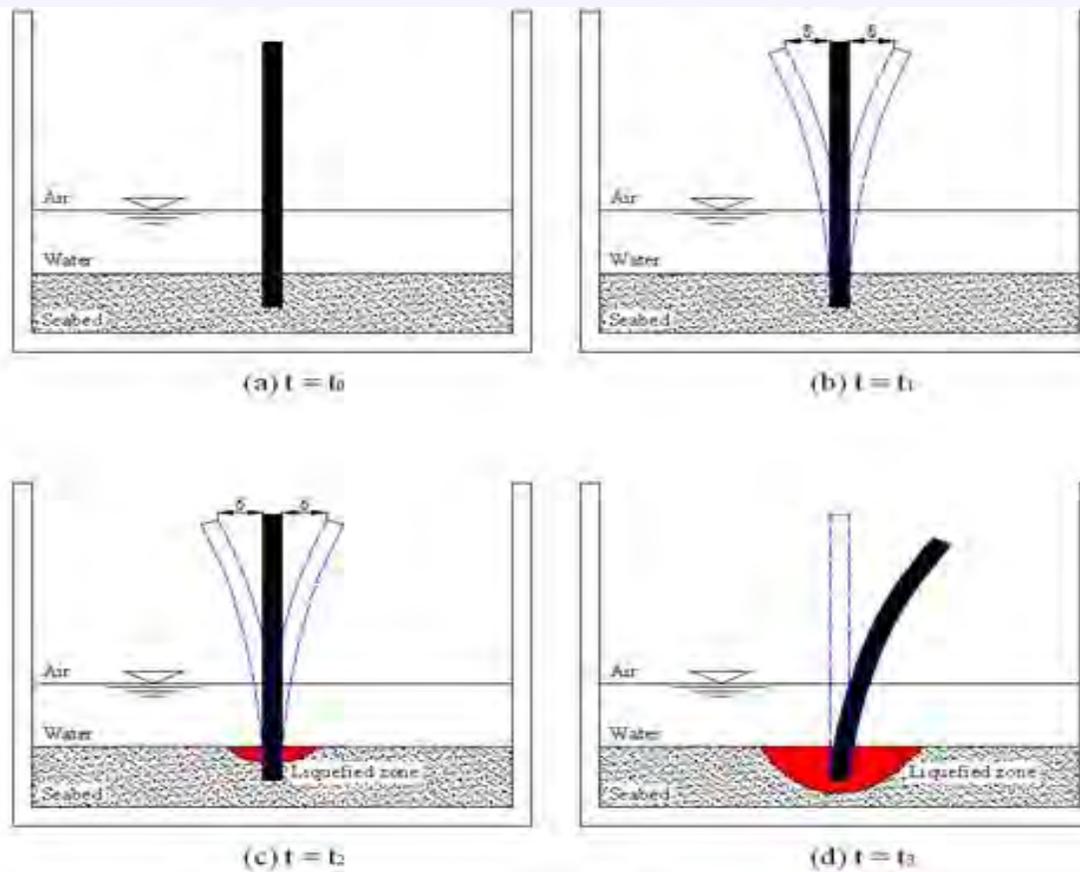
1. Introduction

Foundation of offshore windfarm system

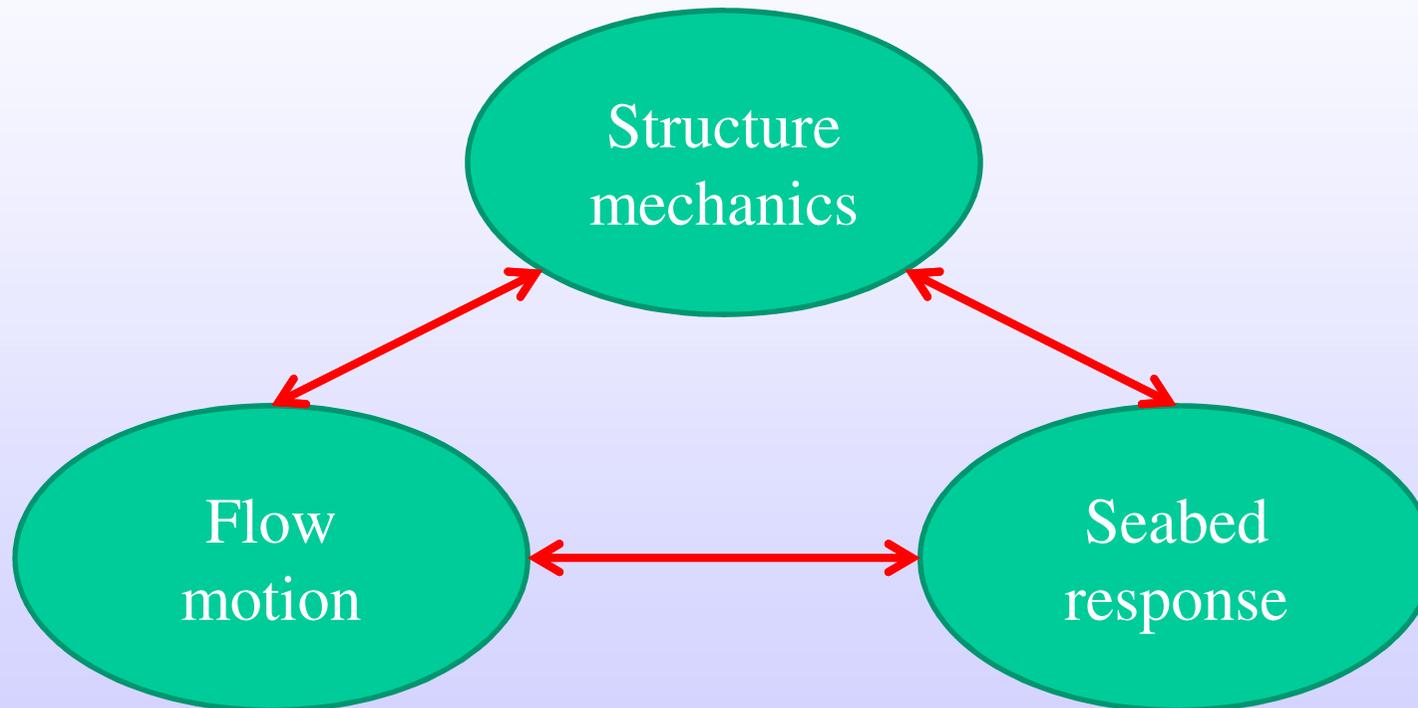


1. Introduction

Rocking of mono-pile structure



2. Theoretical formulations



2. Theoretical formulations

(1) Structure mode

- The structural mechanics theory is based on a weak formulation of the equilibrium equations expressed in the global stress components.

$$-\nabla \cdot \sigma = \vec{F}_m$$

in which \vec{F}_m denotes the periodic volume forces from external wind.



2. Theoretical formulations

(2) Flow mode

- Reynolds-Averaged Navier-Stokes (RANS) equations
- Sponge layer at two sides for damping flow energy

2. Theoretical formulations

(3) Seabed mode

- Biot's poro-elastic theory

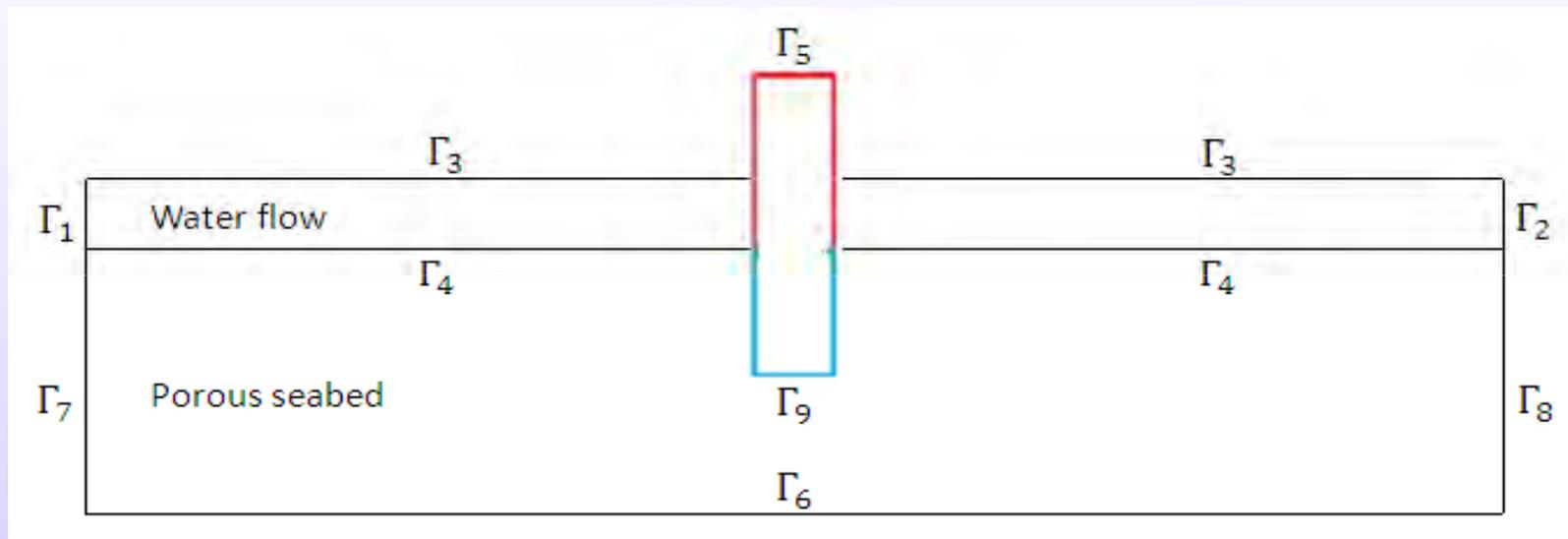
$$\nabla^2 p - \frac{\gamma_w n_s \beta_s}{K} \frac{\partial p}{\partial t} = \frac{\gamma_w}{K} \frac{\partial \varepsilon_s}{\partial t} \quad p: \text{rocking-induced pore pressure}$$

$$G \nabla^2 u_s + \frac{G}{1-2\mu_s} \frac{\partial \varepsilon_s}{\partial x} = \frac{\partial p}{\partial x} \quad u_s: \text{soil displacement in x-direction}$$

$$G \nabla^2 w_s + \frac{G}{1-2\mu_s} \frac{\partial \varepsilon_s}{\partial z} = \frac{\partial p}{\partial z} \quad w_s: \text{soil displacement in z-direction}$$

2. Theoretical formulations

Boundary conditions (conducted in COMSOL)



Γ_1 - 2 : sponge layer; Γ_3 : zero air pressure; Γ_4 : no-slip, flow pressure and shear stress to seabed mode; Γ_5 : no-slip, periodic wind force to structure; Γ_6 : impermeable sea bottom; Γ_7 - 8 : fixed wall; Γ_9 : no-slip, structure deformation to seabed.

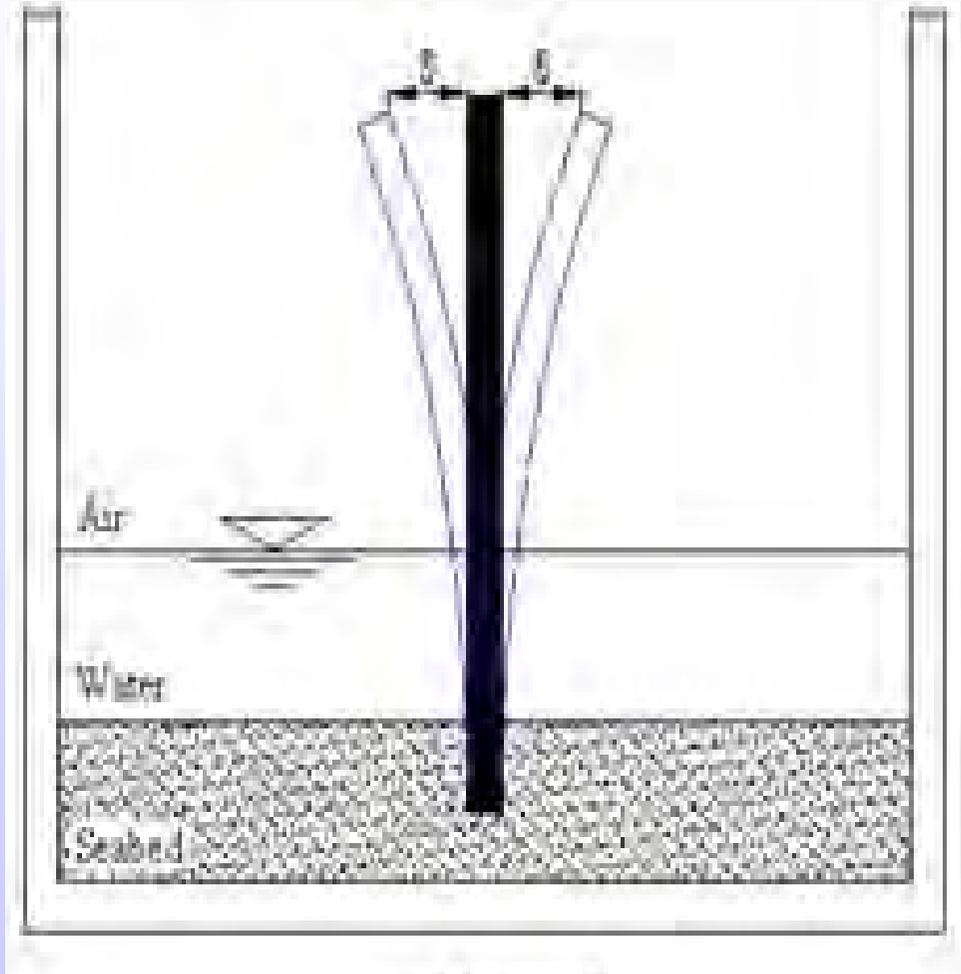
3. Numerical results

Table 1: Structure and soil characteristics

Mono-pile diameter	6 m
Height above sea floor	25 m
Seabed thickness	25 m
Soil porosity	0.3
Shear modulus	10^7 N/m²

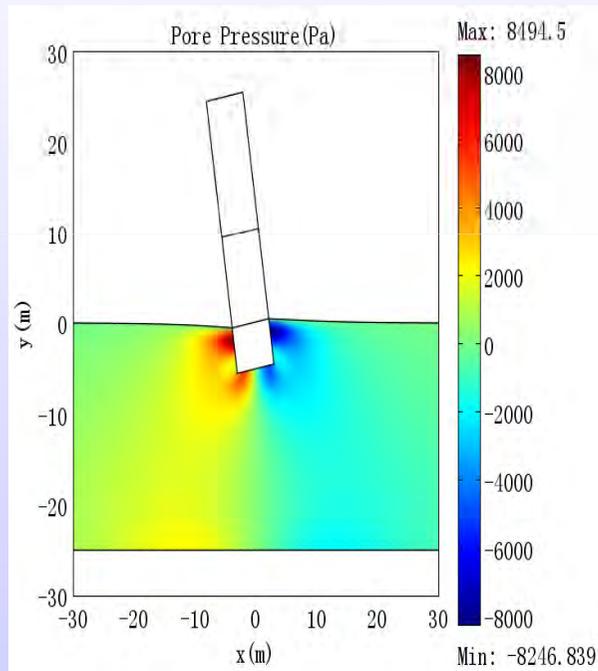
Table 2: Parametric studies

Soil permeability	9.0E-3 ~ 1.5E-2 m/sec
Multi-layer soil	One-layer & two-layer
Degree of saturation	85% ~ 100%
Embedded depth	5.0 ~ 8.0 m
Rocking period	4.0 ~ 8.0 sec
Rocking amplitude	0.05 ~ 0.1 m

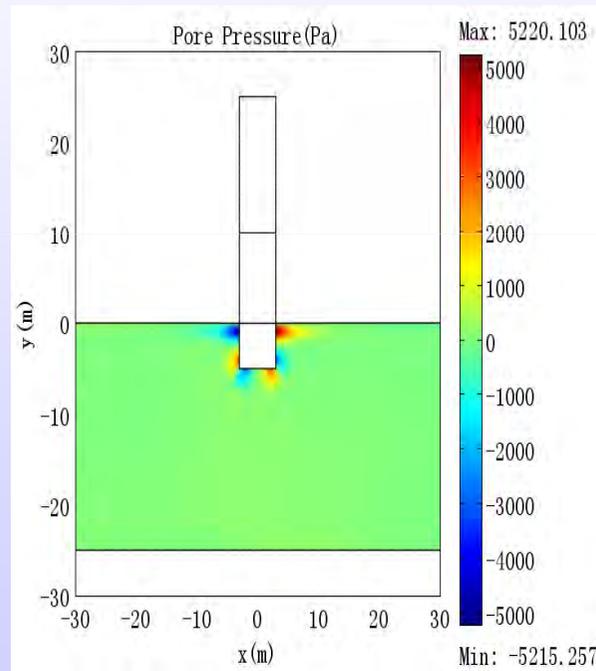


3. Numerical results

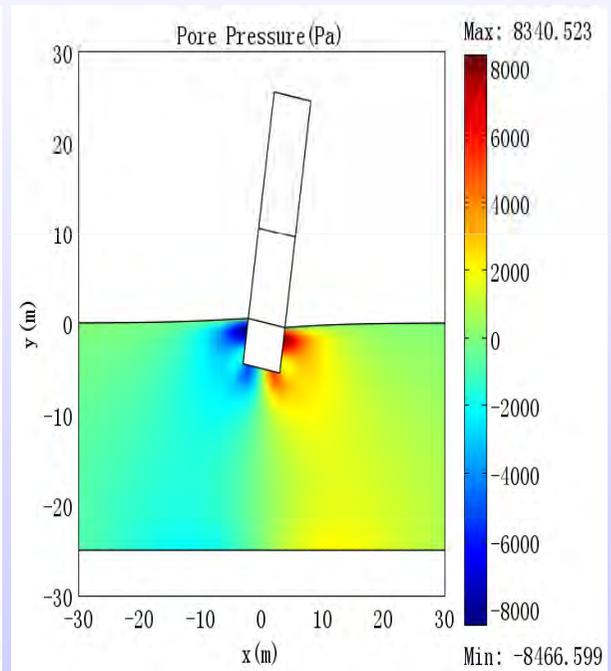
Distribution of rocking-induced pore pressure



$t=T/4$



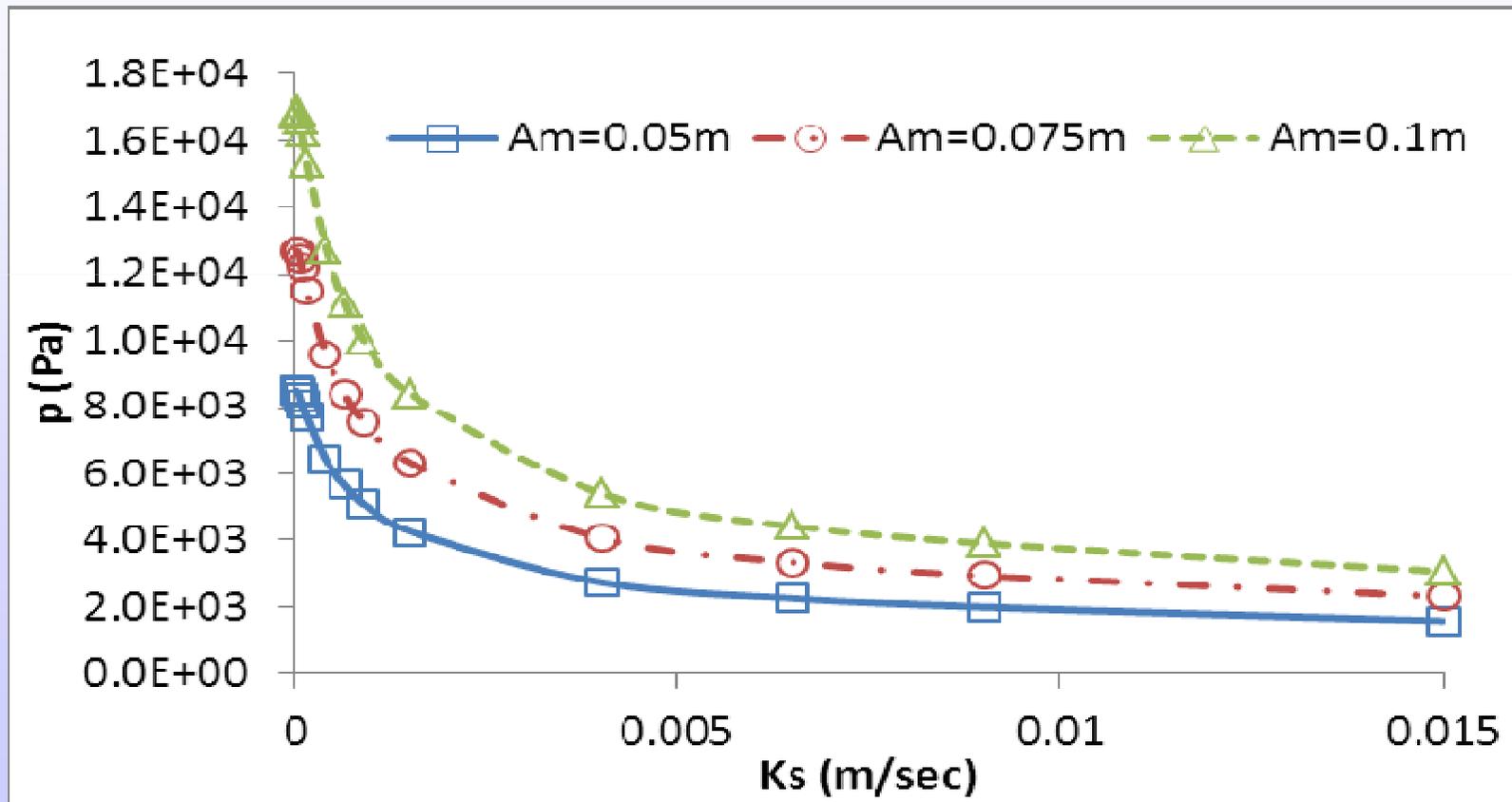
$t=T/2$



$t=3T/4$

3. Numerical results

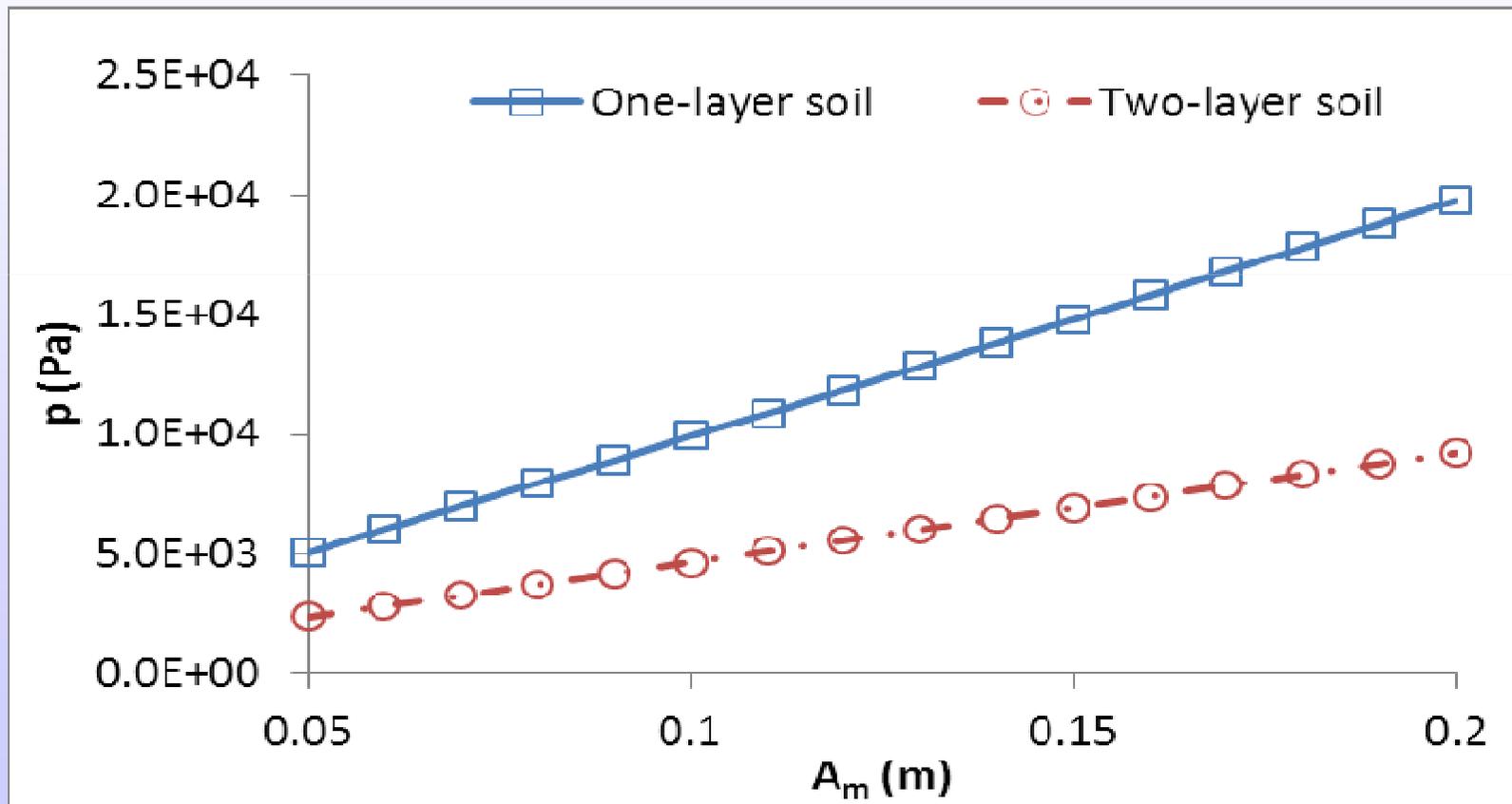
Effect of soil permeability on maximal pore pressure



$S=0.95$

3. Numerical results

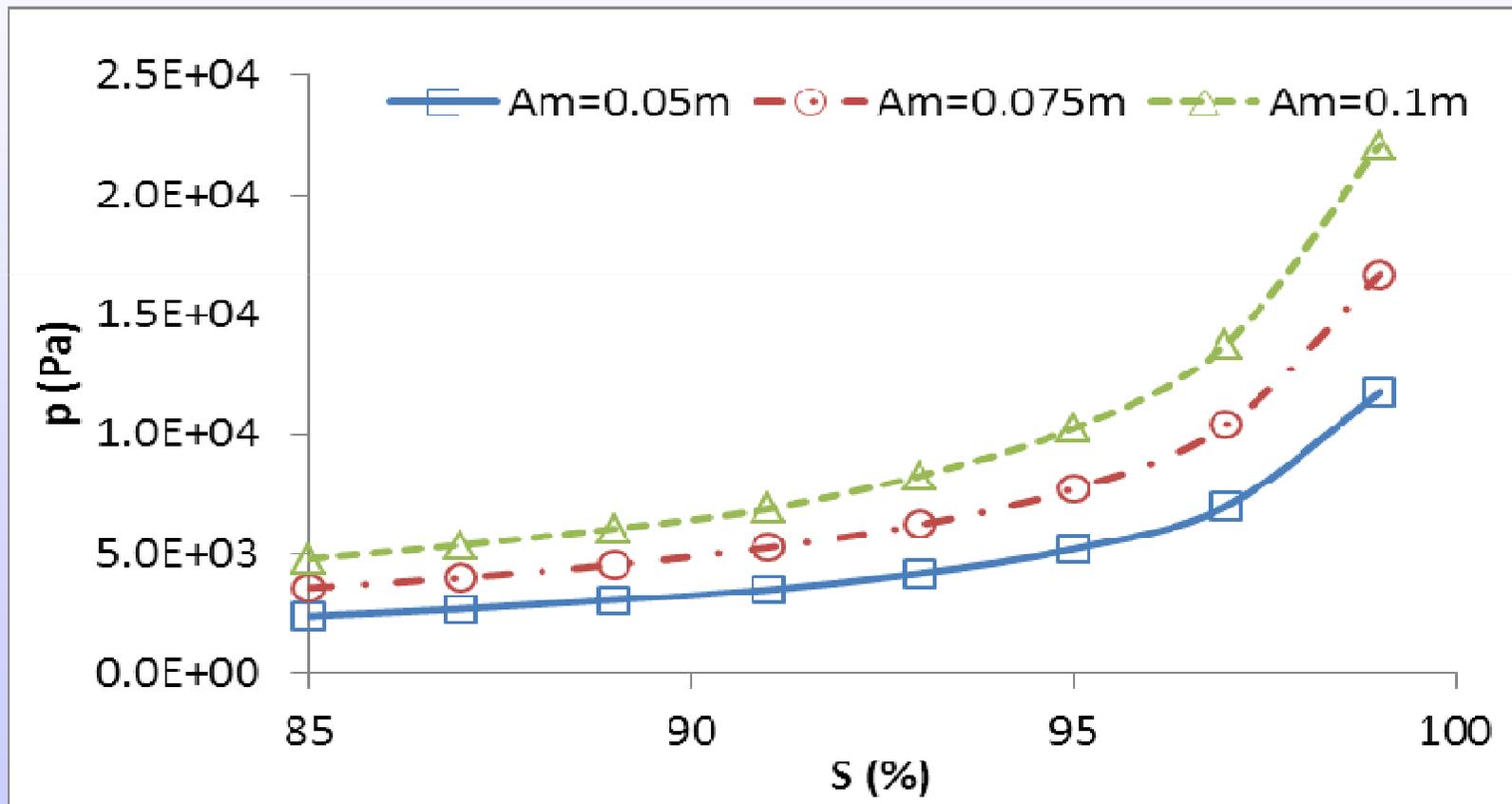
Effect of multi-layer soil on maximal pore pressure



Upper 2m soil with $K_s=9.0E-3m/sec$ and the rest with $K_s=8.4E-4m/sec$

3. Numerical results

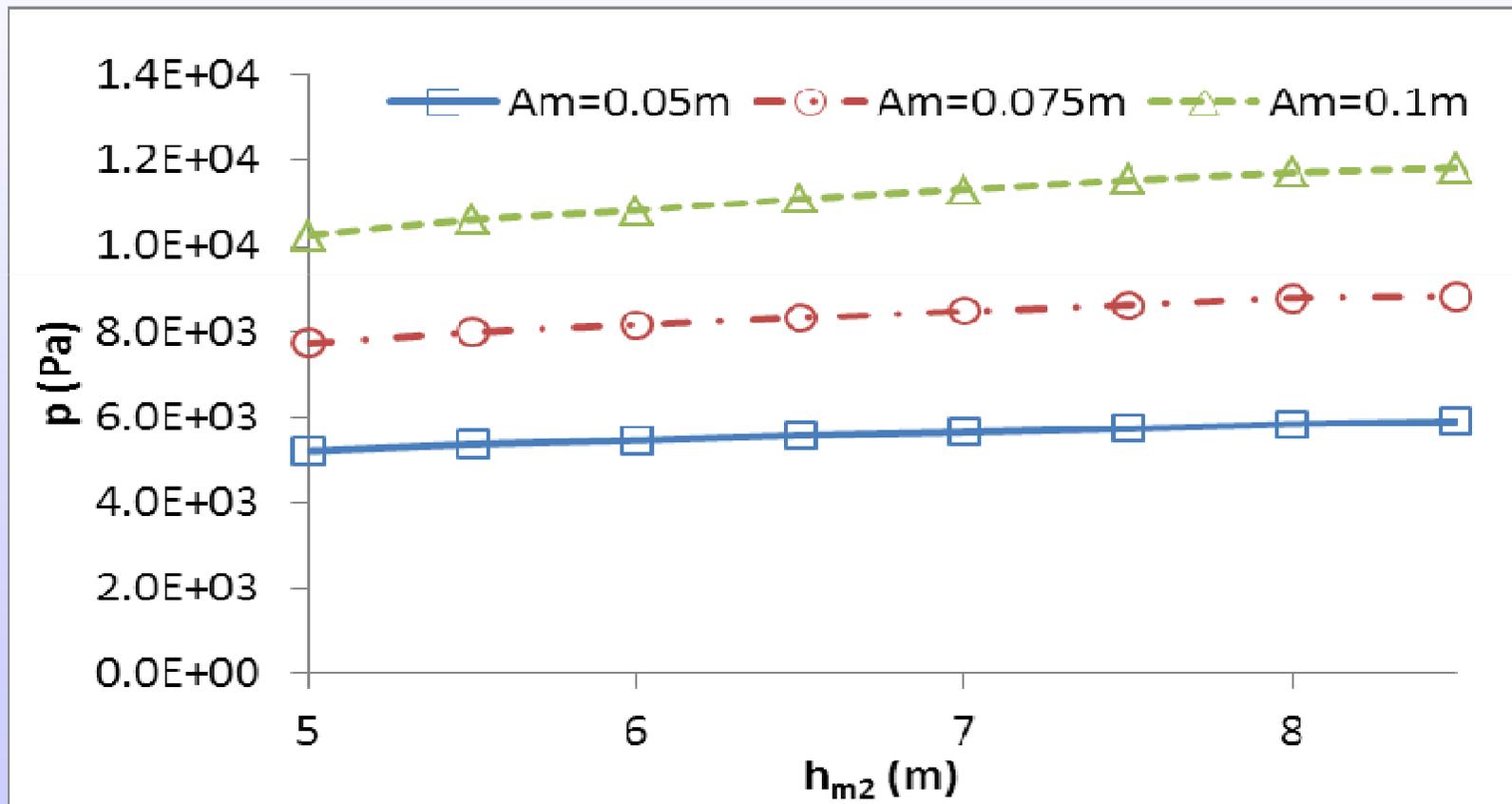
Effect of saturation degree on maximal pore pressure



$K_s = 8.4\text{E-}4\text{m/sec}$

3. Numerical results

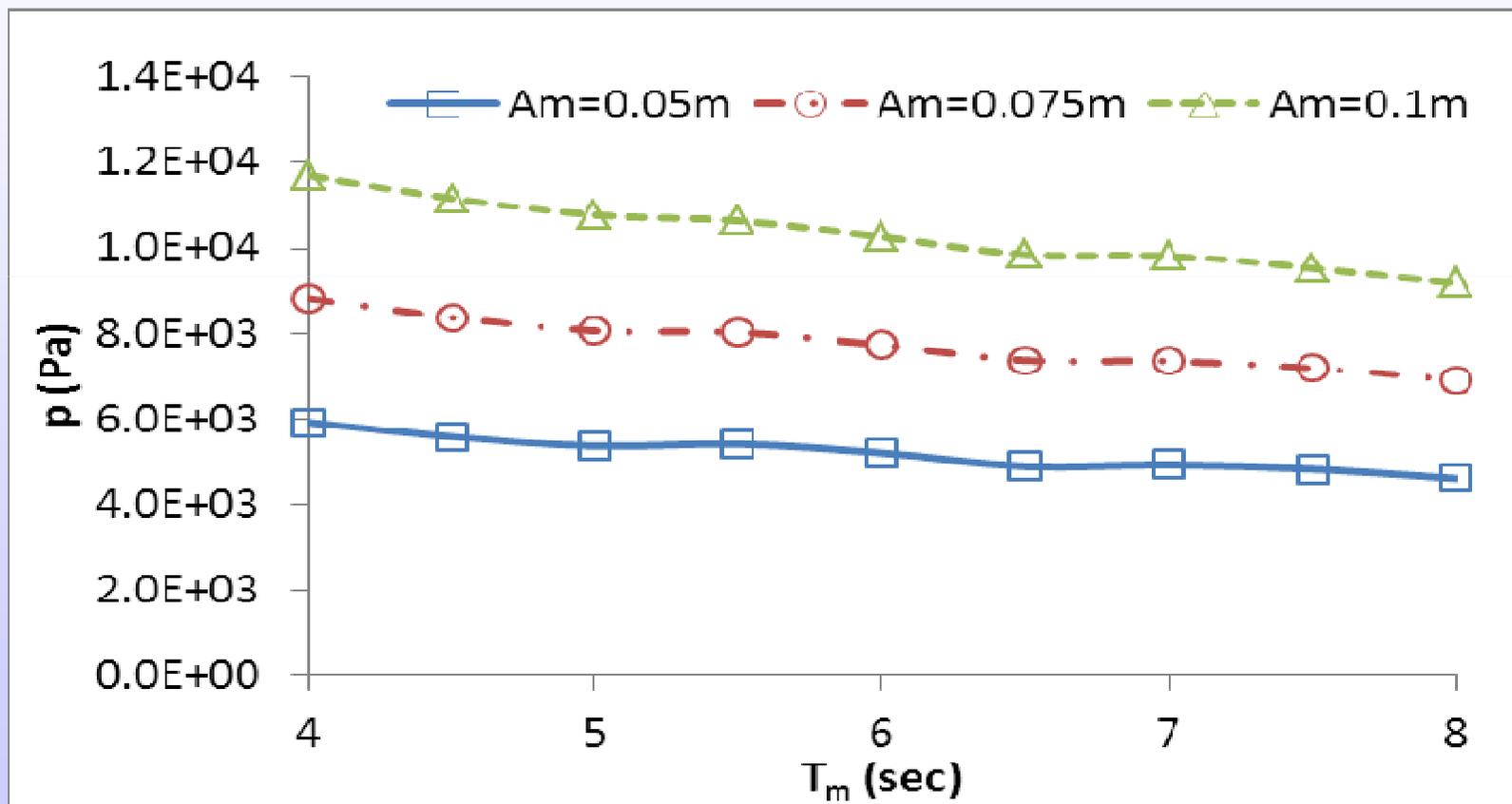
Effect of embedded depth on maximal pore pressure



$S=0.95$ and $K_s=8.4E-4m/sec$

3. Numerical results

Effect of rocking period on maximal pore pressure



$S=0.95$ and $K_s=8.4E-4m/sec$

4. Conclusions & future work

- The COMSOL Multiphysics has a good potential in modeling the rocking-induced seabed response.
- The seabed properties, structure dimensions and rocking parameters may significantly affect the rocking-induced maximal pore pressure.
- Further development and detailed validation of this integrated model are needed.



Many thanks for your attention!