

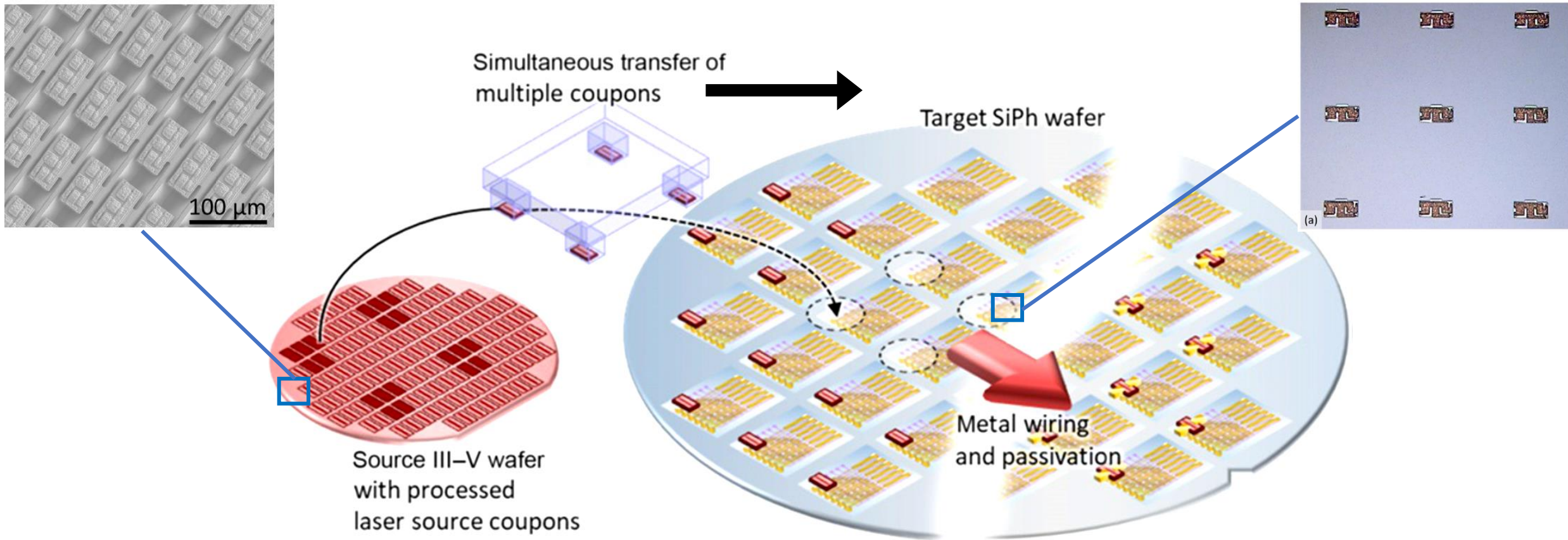
Temperature Effects on Thermomechanical Properties of Elastomeric Stamps for Micro Transfer Printing Applications

C. Reyes

9/29/2020

What is Micro Transfer Printing - μ TP?

Micro-transfer printing (μ TP) enables mass-transfer of wafer-level chips having lateral dimensions ranging from $3 \times 7 \mu\text{m}$ to $650 \times 650 \mu\text{m}$ to a nonnative target wafer. .

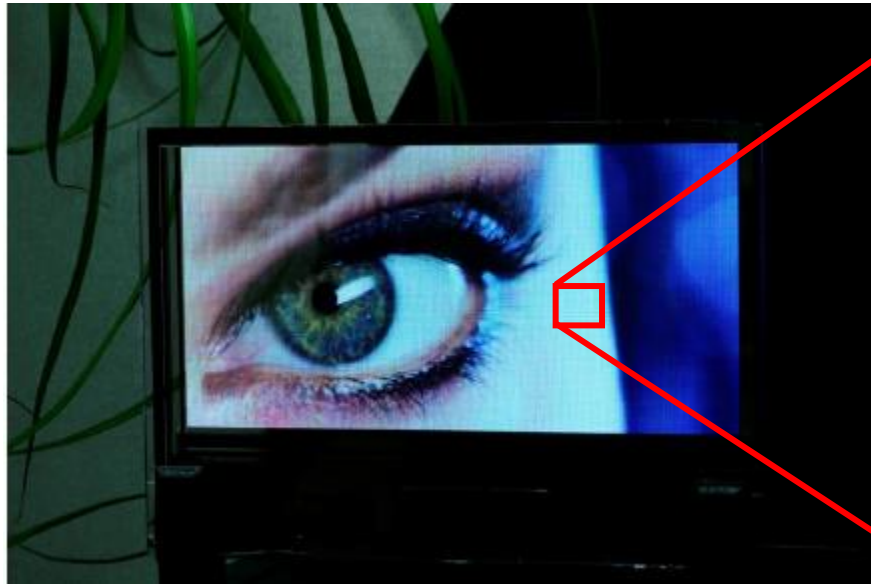


Corbett, Brian, et al. "Transfer printing for silicon photonics." *Semiconductors and Semimetals*. Vol. 99. Elsevier, 2018. 43-70.

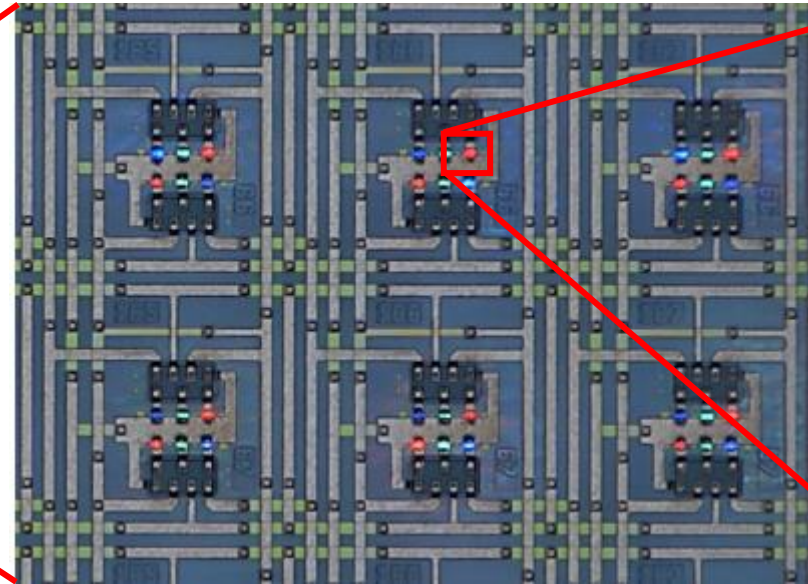
Applications of μ TP

Micro-transfer printing (μ TP) enables mass-transfer of wafer-level chips having lateral dimensions ranging from $3 \times 7 \mu\text{m}$ to $650 \times 650 \mu\text{m}$ to a nonnative target wafer. Applications include, solar junctions, lasers, optical devices, LEDs etc.

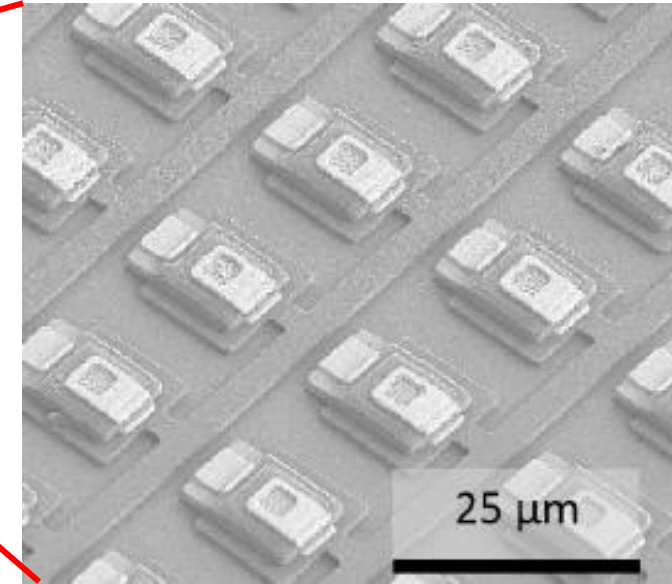
5.1", 70 PPI MicroLED



Printed MicroLEDs and IC Drivers



MicroLEDs

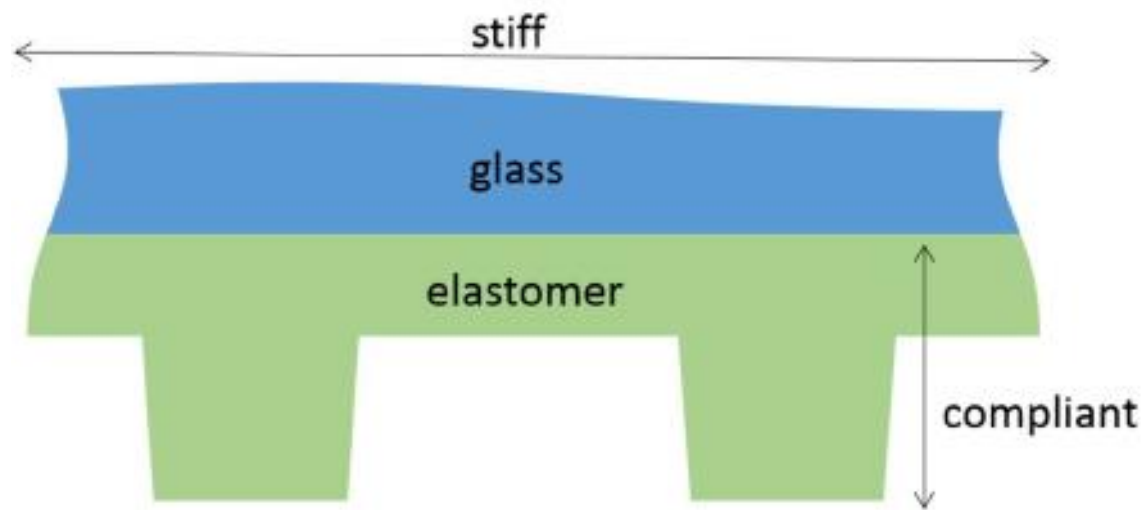


Bower, C. A., et al. "Emissive displays with transfer-printed microscale LEDs and ICs." *Light-Emitting Devices, Materials, and Applications XXIV*. Vol. 11302. International Society for Optics and Photonics, 2020.

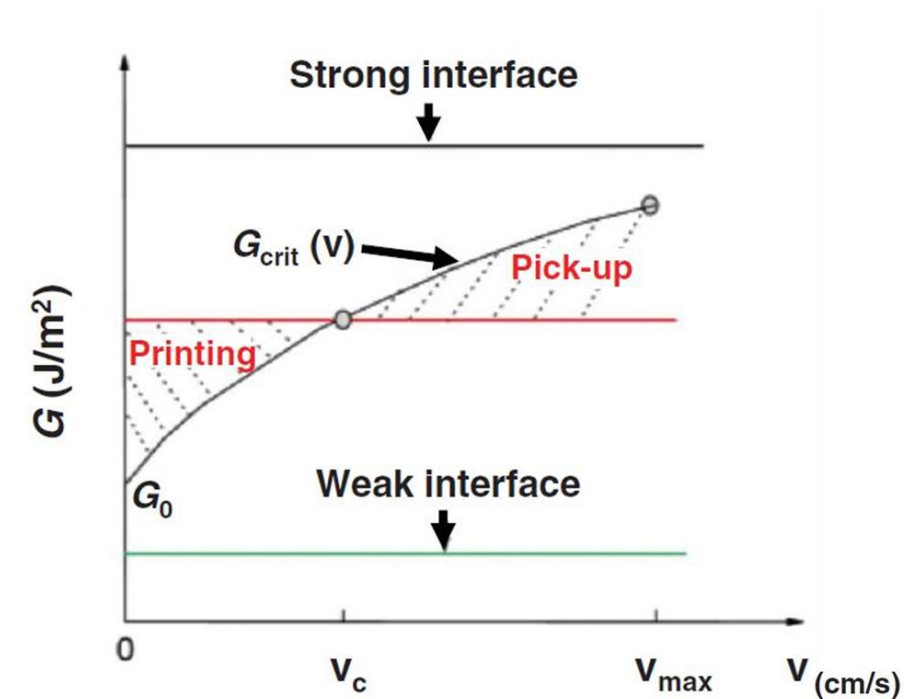
How μ TP Works – PDMS Elastomer Stamp

The viscoelastic properties of PDMS allow for kinetic control of adhesion as the stamp/source as the release energy is controlled by the speed of the stamp.

Stamp Cross Section



Release Energy vs Stamp Speed



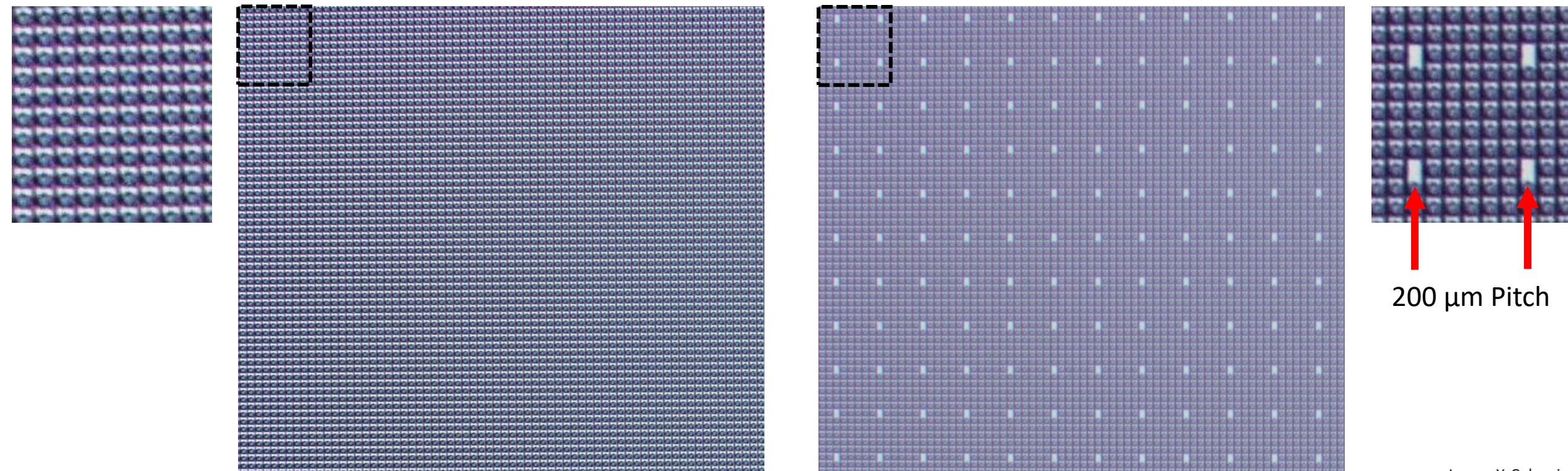
Carlson, Andrew, et al. "Transfer printing techniques for materials assembly and micro/nanodevice fabrication." *Advanced Materials* 24.39 (2012): 5284-5318.

Gomez, David, et al. "Scalability and yield in elastomer stamp micro-transfer-printing." *2017 IEEE 67th Electronic Components and Technology Conference (ECTC)*. IEEE, 2017.

Challenges with μ TP – Thermal Expansion

- To enable the printing of high-density small devices, the picking and placement accuracy needs to be within $\pm 1.5 \mu\text{m}$ alignment error.
- During extended printing, the temperature inside the μ T Printer can increase, leading to thermal expansion of the stamp and decrease placement accuracy.
- *The stamp used for the printing array shown below will be used as the geometric model.*

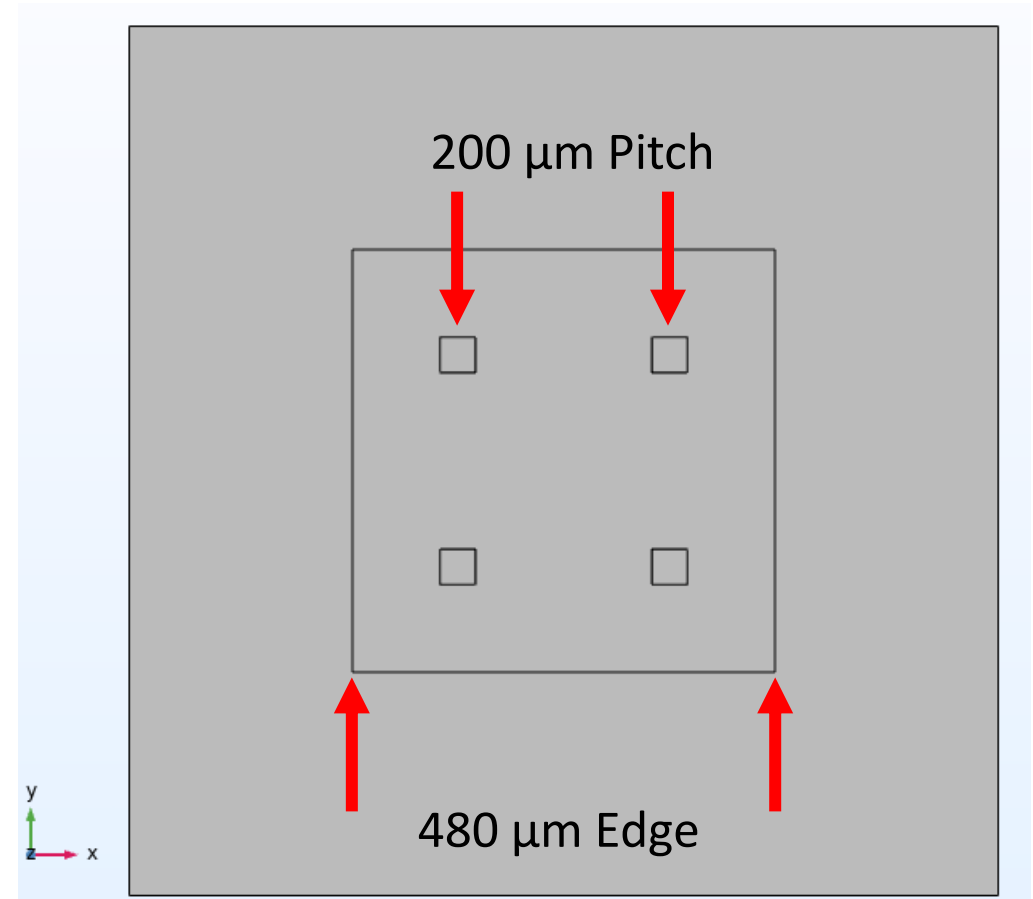
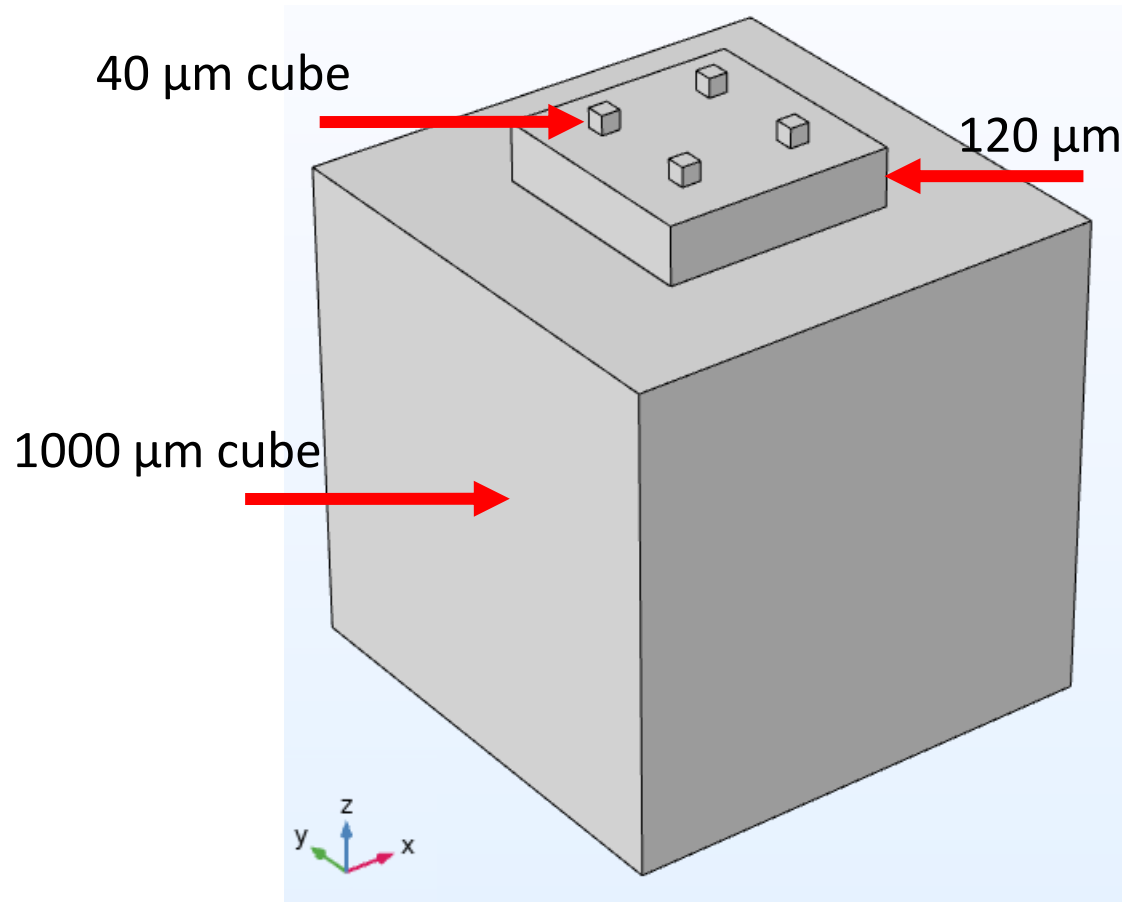
High Density Array of Devices Before and After μ TP

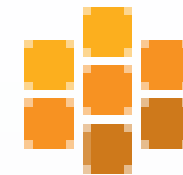




Geometry of the PDMS Stamp

- The model consists of a cubic base, rectangular prism intermediate layer and 4 micro posts.
- The material used is PDMS – Polydimethylsiloxane
- *3D model design based on stamp used in previous slide.*



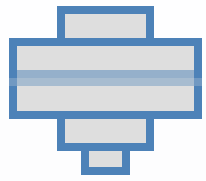


PDMS Materials Properties

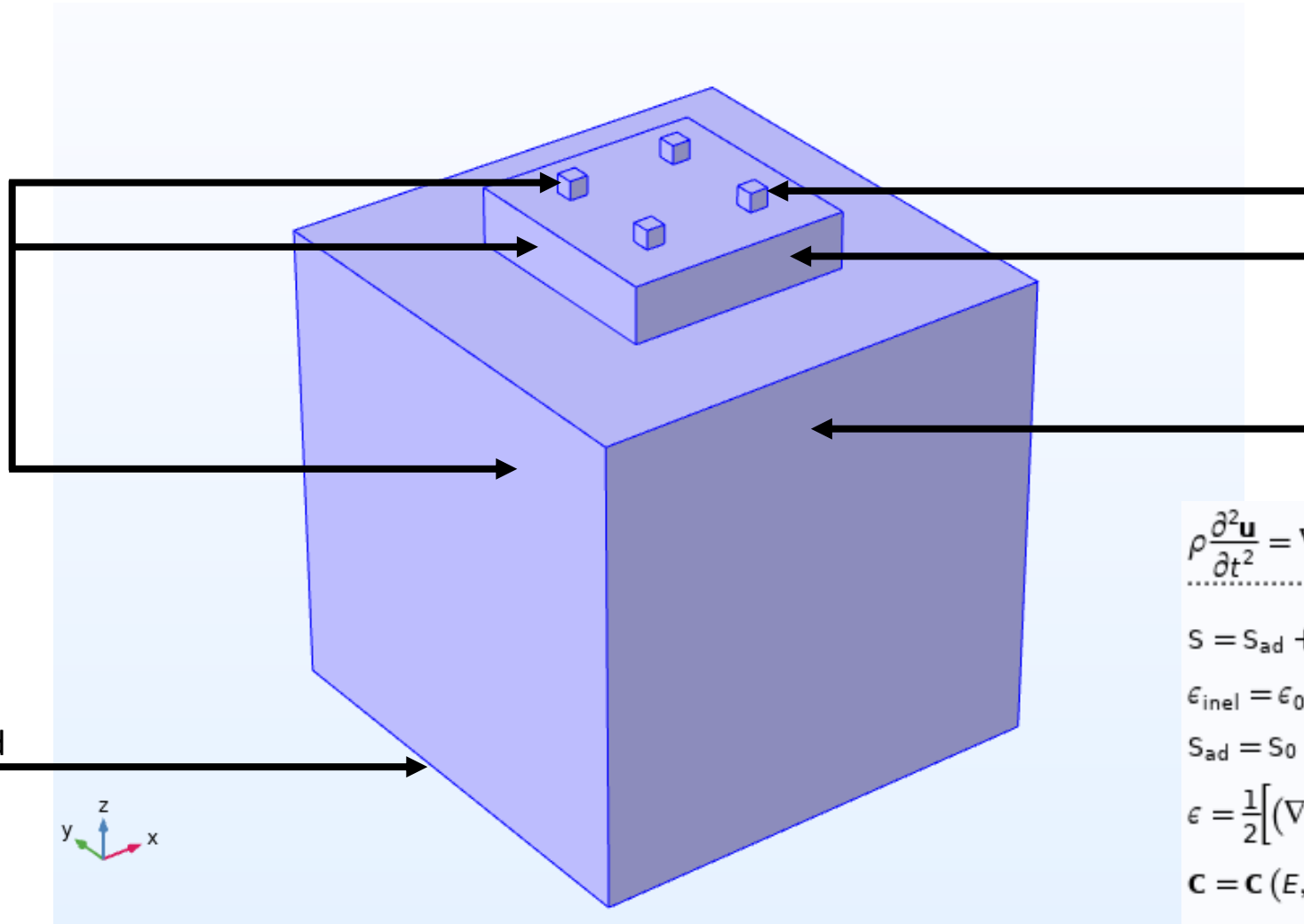
- The following model properties were used in the simulation, see table below.
- Values agree with literature.

Table 1 – Material Properties

Property	Variable	Value	Unit	Property Group
Coefficient of thermal expansion	α_{iso} ; $\alpha_{iij} = \alpha_{iso}$, $\alpha_{ijj} = 0$	$9e-4[1/K]$	1/K	Basic
Heat capacity at constant pressure	C_p	$1460[J/(kg \cdot K)]$	$J/(kg \cdot K)$	Basic
Density	ρ	$970[kg/m^3]$	kg/m^3	Basic
Thermal conductivity	k_{iso} ; $k_{ii} = k_{iso}$, $k_{ij} = 0$	$0.16[W/(m \cdot K)]$	$W/(m \cdot K)$	Basic
Young's modulus	E	$750[kPa]$	Pa	Young's modulus and Poisson's ratio
Poisson's ratio	ν	0.49	1	Young's modulus and Poisson's ratio
Relative permittivity	$\epsilon_{r_{iso}}$; $\epsilon_{r_{ii}} = \epsilon_{r_{iso}}$, $\epsilon_{r_{ij}} = 0$	2.75	1	Basic



Solid Mechanics – Boundary Conditions



All 3 Domains are *Linear Elastic*

All boundaries above base are *Free*

Linear Elastic Equations

Base boundary is *fixed* to replicate a stamp mounted on glass

$$\rho \frac{\partial^2 \mathbf{u}}{\partial t^2} = \nabla \cdot \mathbf{S} + \mathbf{F}_v$$

$$\mathbf{S} = \mathbf{S}_{ad} + \mathbf{C} : \boldsymbol{\epsilon}_{el}, \quad \boldsymbol{\epsilon}_{el} = \boldsymbol{\epsilon} - \boldsymbol{\epsilon}_{inel}$$

$$\boldsymbol{\epsilon}_{inel} = \boldsymbol{\epsilon}_0 + \boldsymbol{\epsilon}_{ext} + \boldsymbol{\epsilon}_{th} + \boldsymbol{\epsilon}_{hs} + \boldsymbol{\epsilon}_{pl} + \boldsymbol{\epsilon}_{cr} + \boldsymbol{\epsilon}_{vp}$$

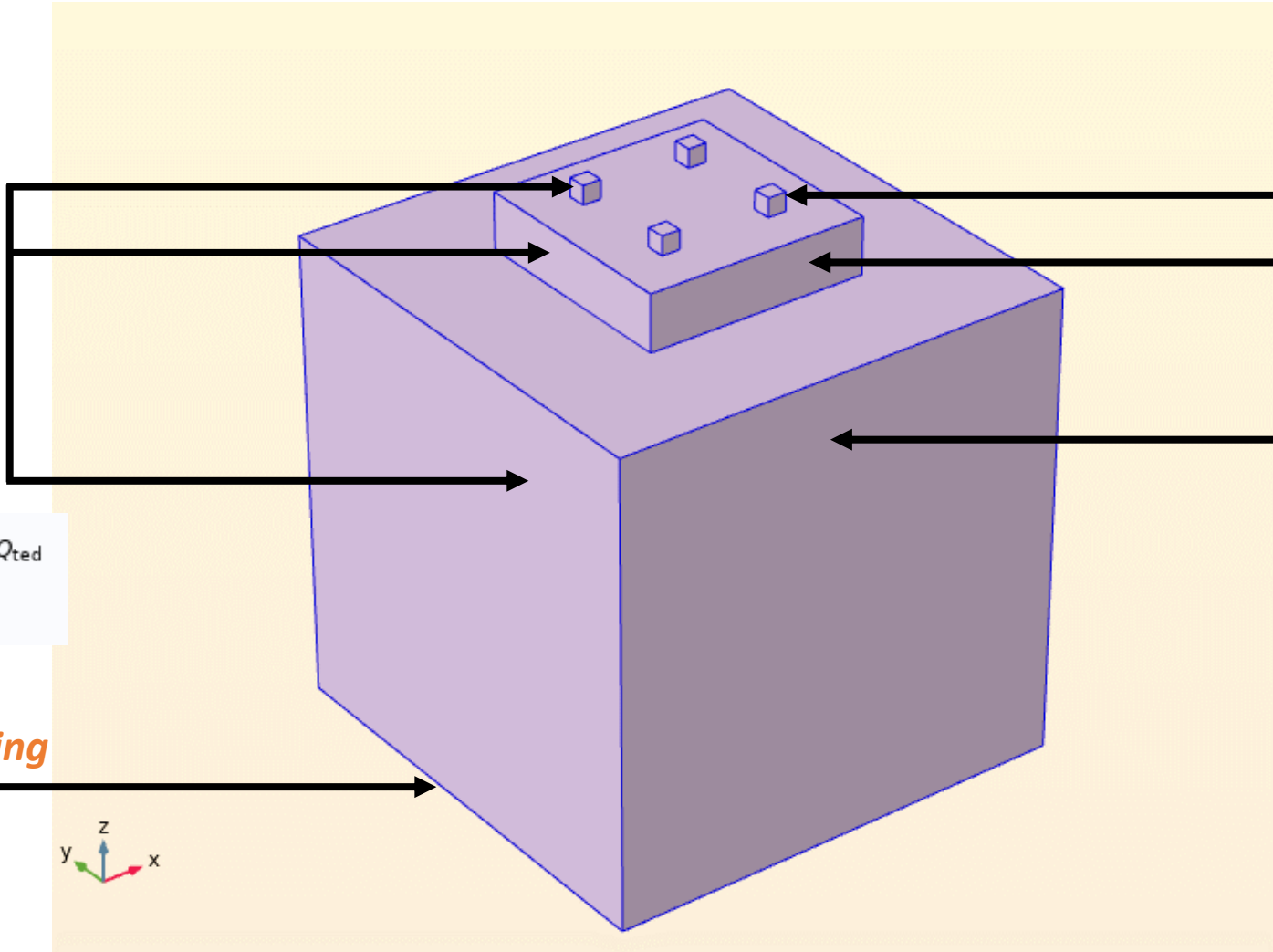
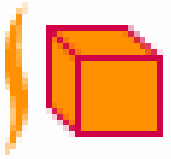
$$\mathbf{S}_{ad} = \mathbf{S}_0 + \mathbf{S}_{ext} + \mathbf{S}_q$$

$$\boldsymbol{\epsilon} = \frac{1}{2} [(\nabla \mathbf{u})^T + \nabla \mathbf{u}]$$

$$\mathbf{C} = \mathbf{C}(E, \nu)$$



Heat Transfer in Solids– Boundary Conditions



All 3 Domains are **Solid**

All boundaries above base are set to **Convective Heat Flux**

Solid Heat Equations

Heat Flux Equations

$$\rho C_p \frac{\partial T}{\partial t} + \rho C_p \mathbf{u} \cdot \nabla T + \nabla \cdot \mathbf{q} = Q + Q_{\text{ted}}$$

$$\mathbf{q} = -k \nabla T$$

$$-\mathbf{n} \cdot \mathbf{q} = q_0$$

$$q_0 = h(T_{\text{ext}} - T)$$

- $T_{\text{initial}} = 293.15 \text{ K}$
- $T_{\text{ext}} = 350.15 \text{ K}$
- h , heat transfer coefficient
 - 1 W/m^2

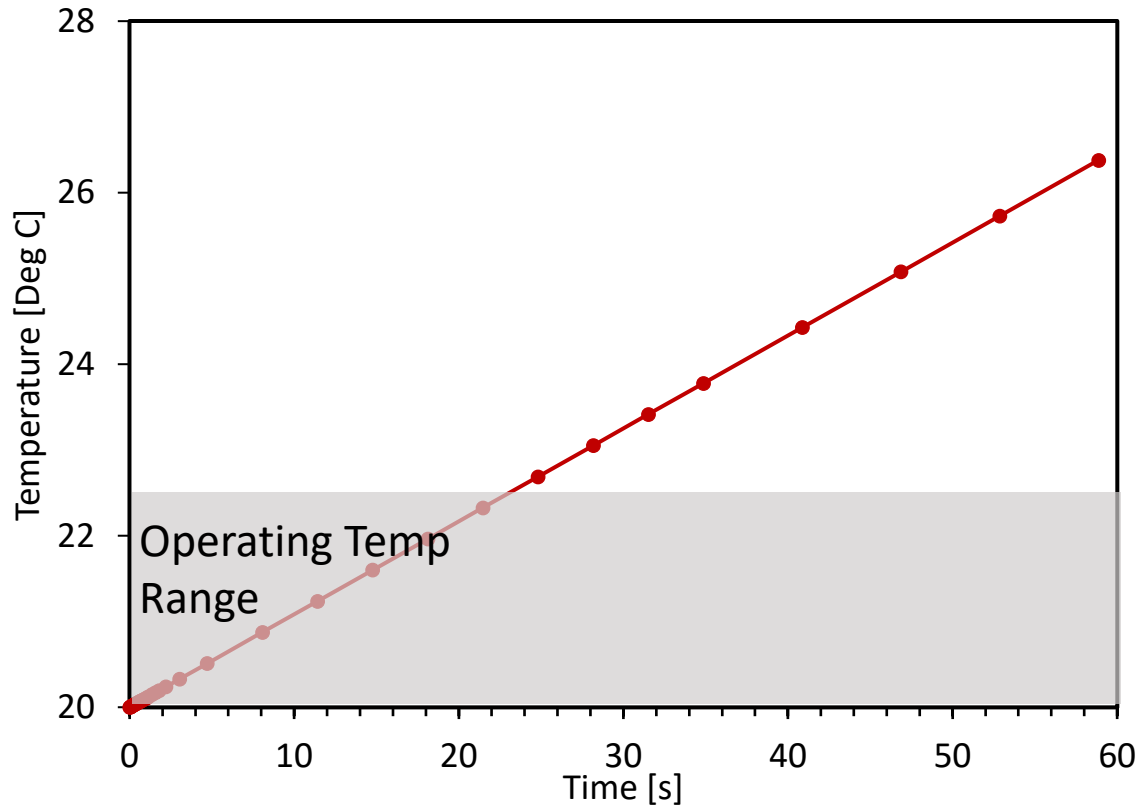
Base boundary is **Insulating**



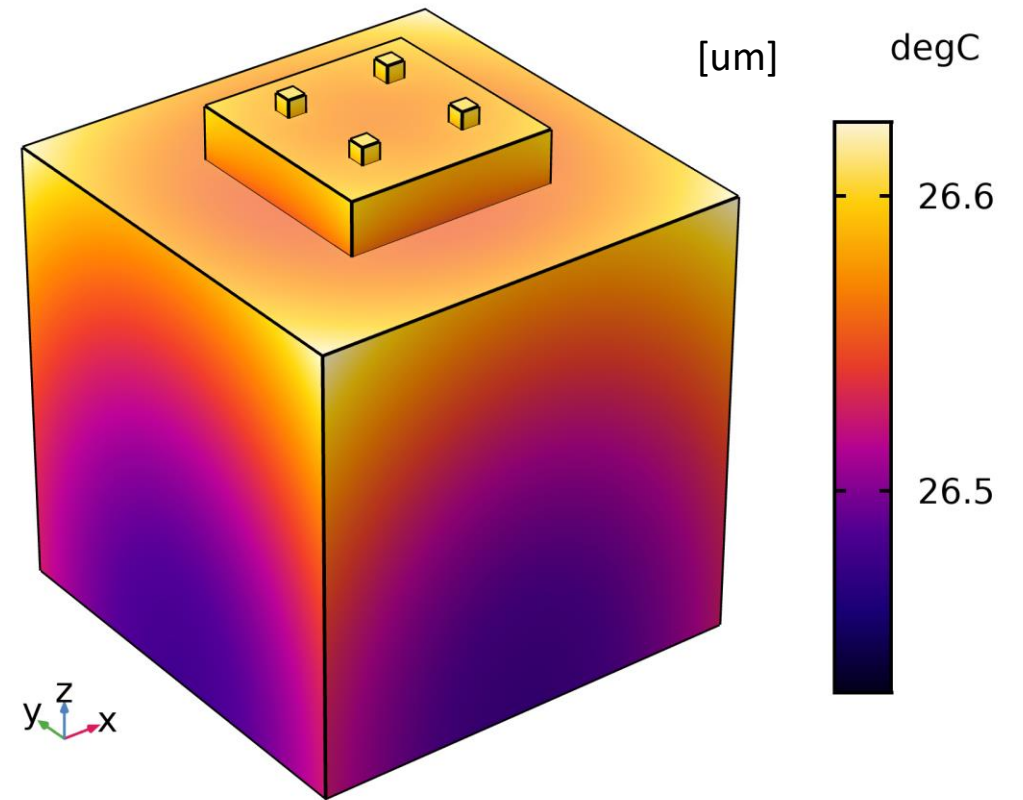
*All initial \mathbf{u} and $\delta^2 \mathbf{u} / \delta t^2$ values set to **Zero**.

Results – Surface Temperature

Average Surface Temperature vs Time

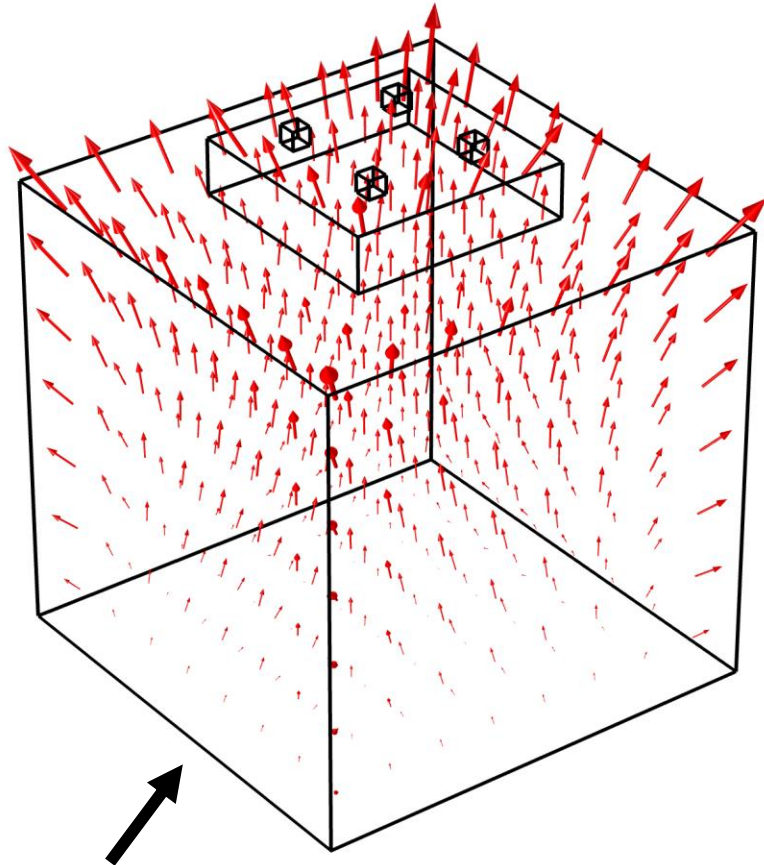


Surface Temperature @ ~60s



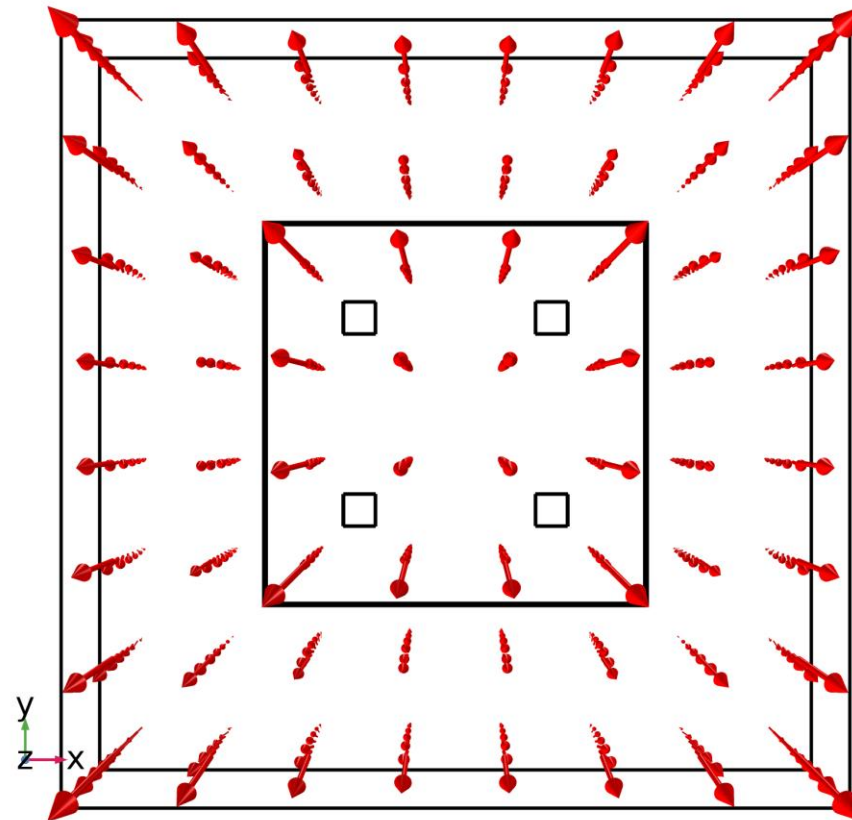
Direction of Volume Displacement

- Volume displacement vector arrows are plotted in an 8 x 8 array and are proportional to the displacement field.
- Displayed arrow is at the end of the simulation ~60 s.



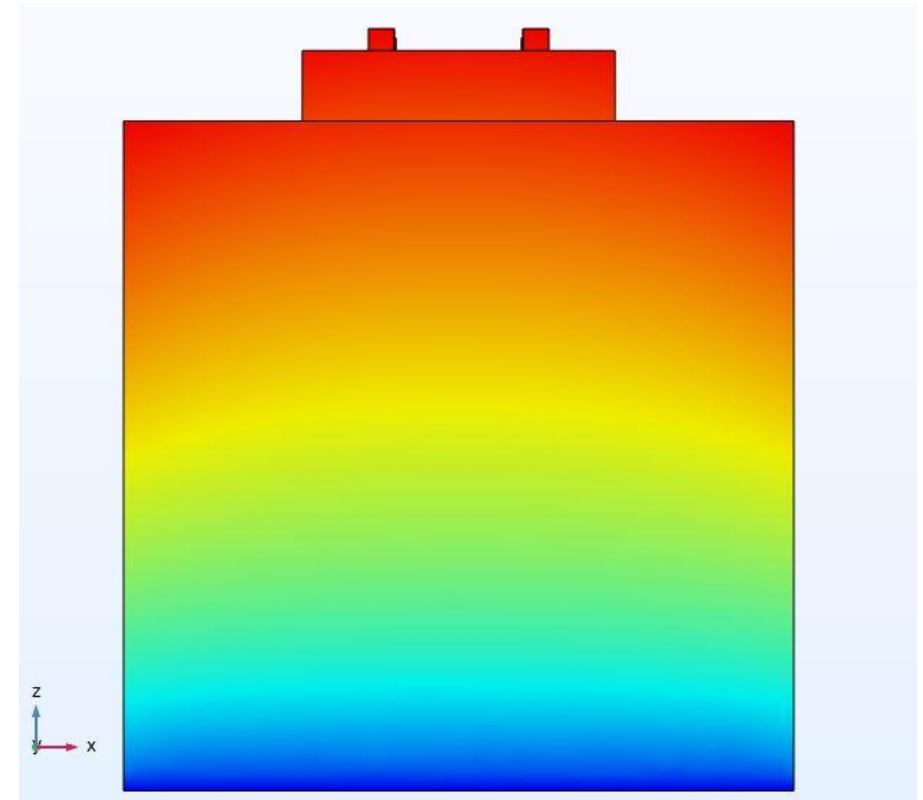
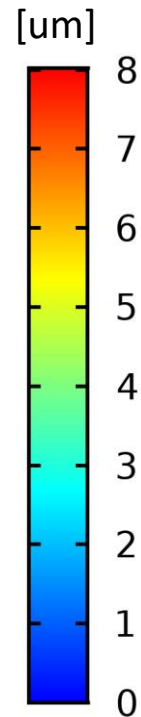
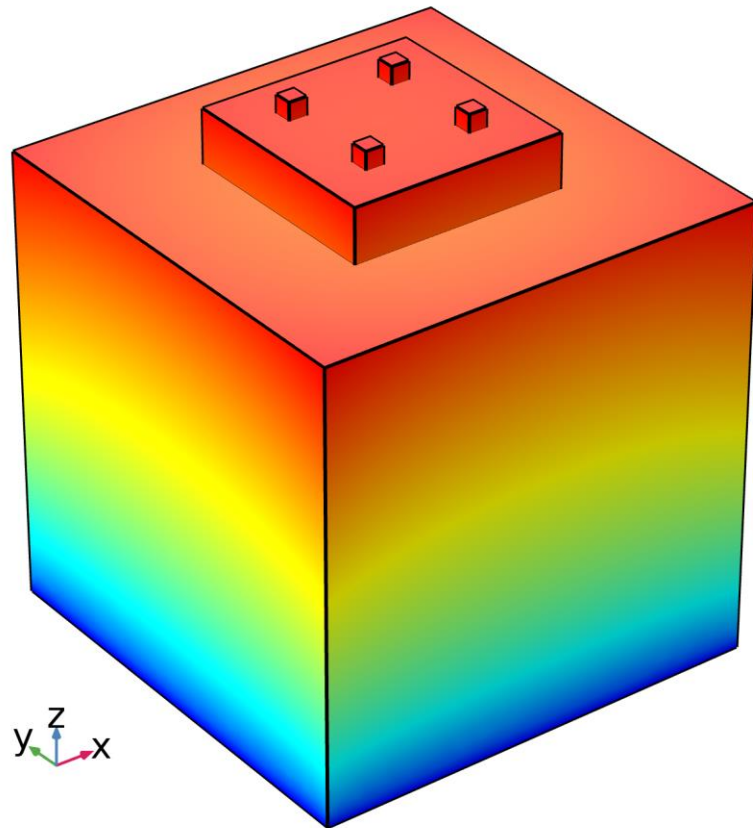
Movement lower at base because of fixed constraint

Expansion movement is outward from center and is larger at corners of the base and intermediate layers.



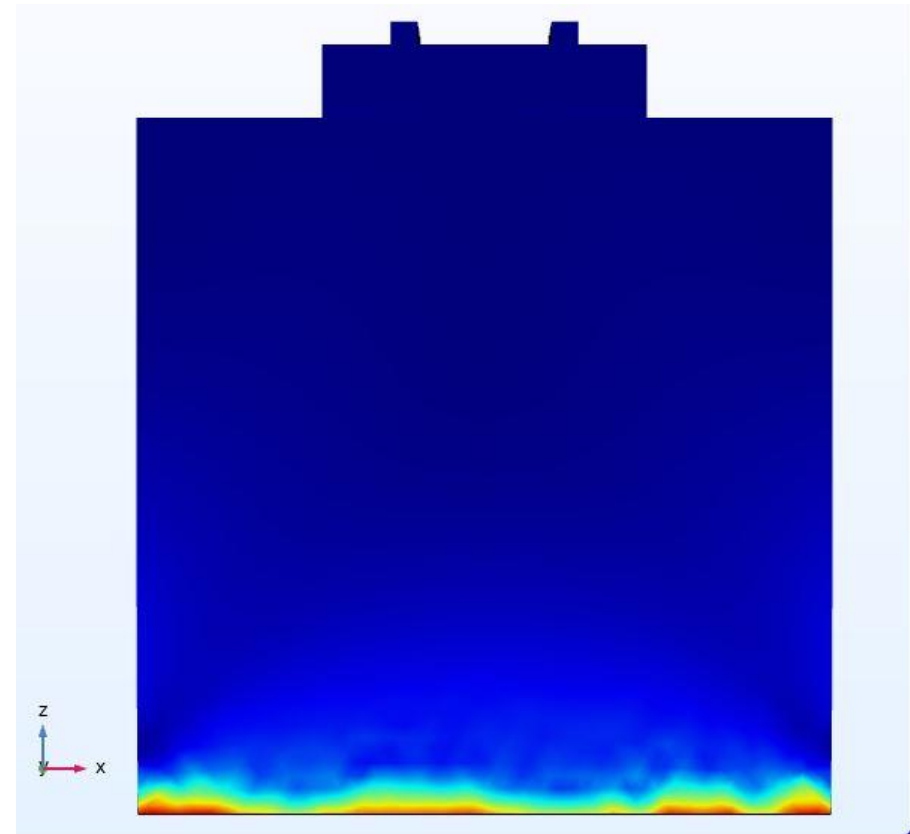
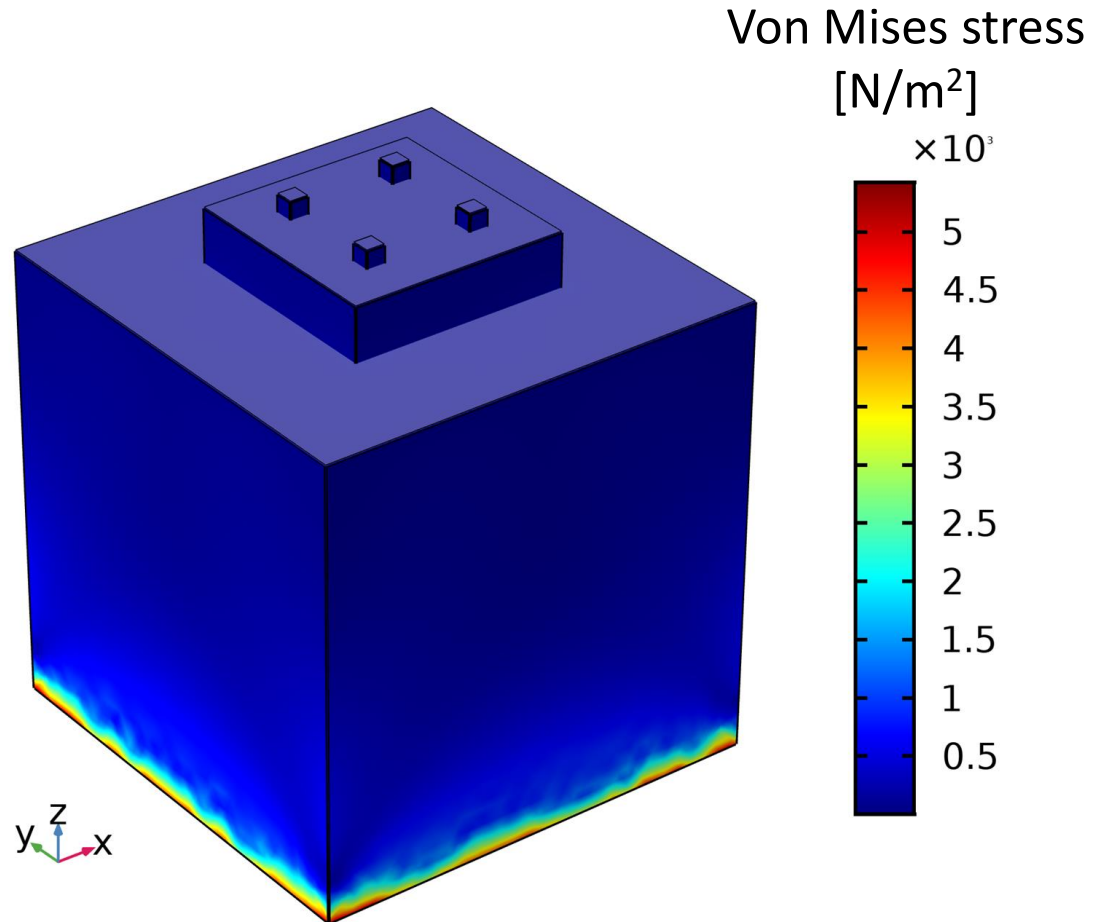
Total Average Displacement

Plotted is the total volume displacement at the end of the simulation. The fixed constraint minimizes the bottom movement, while the upper portion of the stamp moves upwards and outwards as seen in the volume arrow directions.



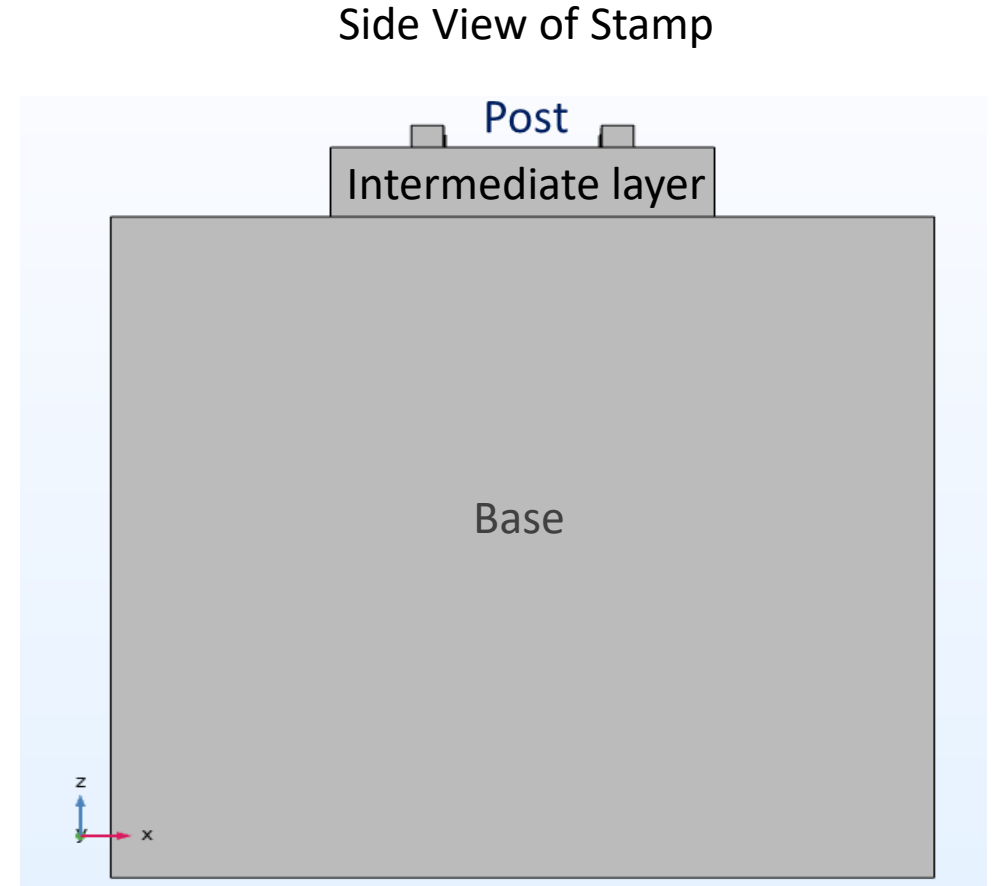
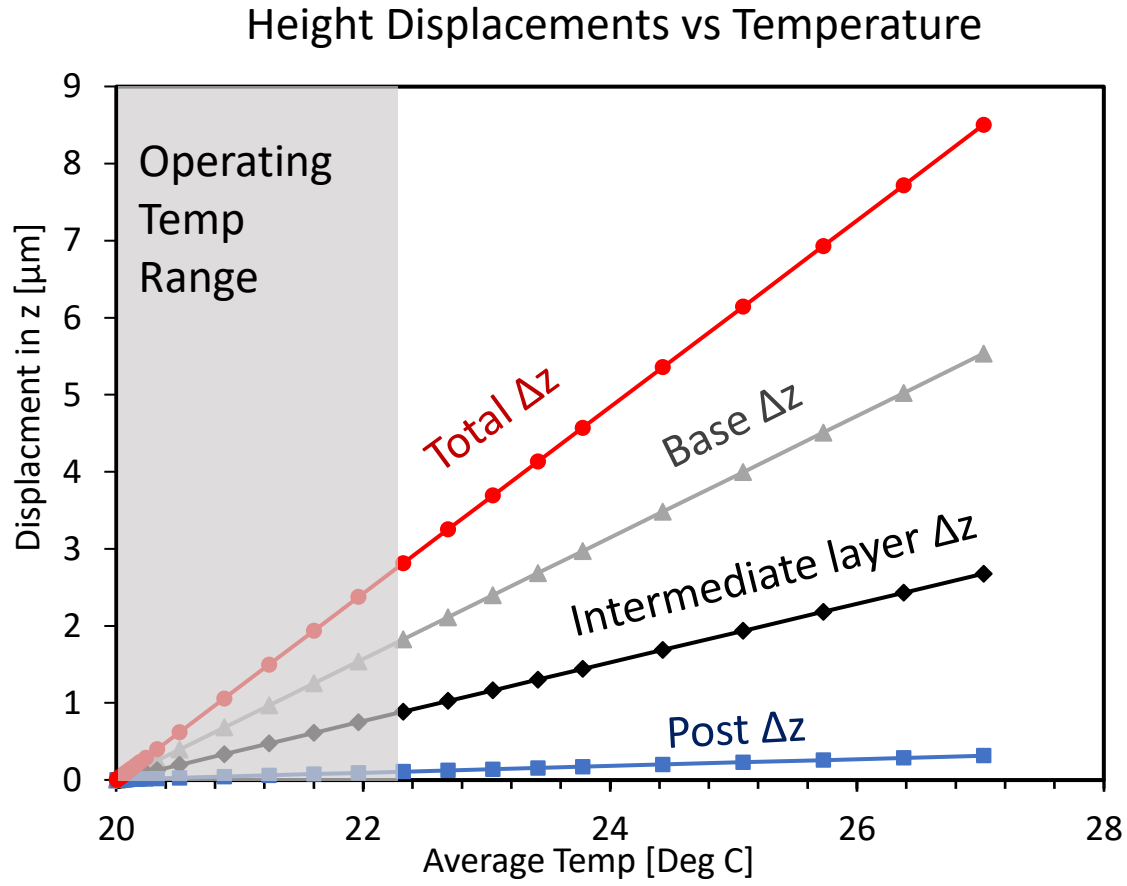
Von Mises Stress

Plotted are the Von Mises Stresses at the end of the simulation. They are concentrated at the base where the fixed condition is imposed and diminish rapidly towards the top of the elastomer stamp.

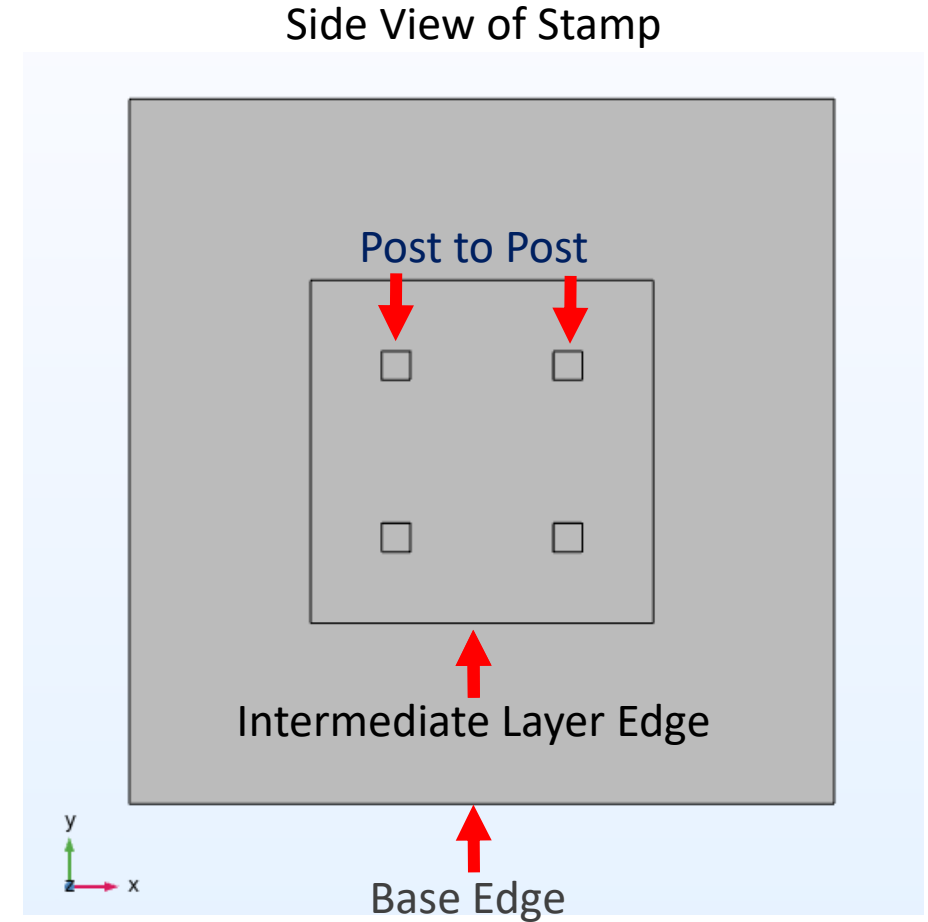
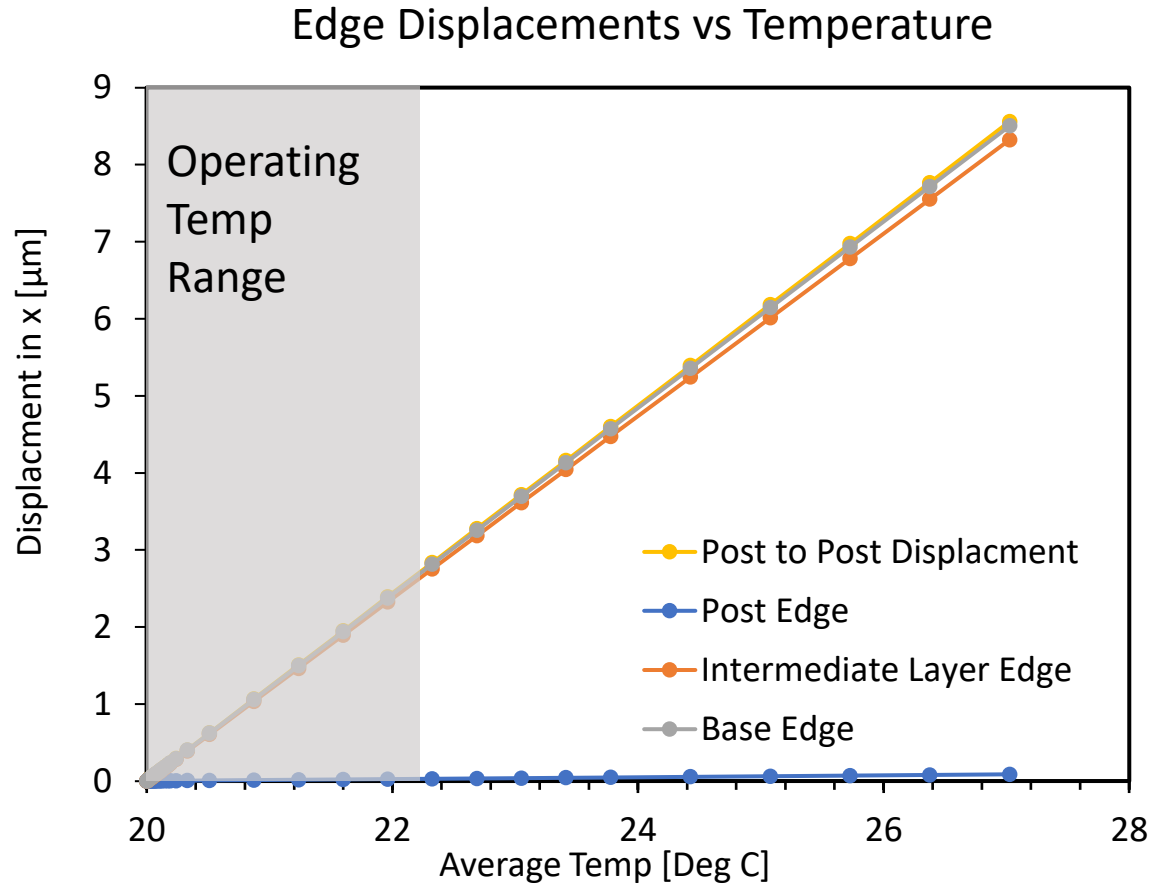


C. Reyes X-Celeprint

Results – Vertical Displacement



Results – Lateral Displacement



Conclusions Future Work

- Near room temperature (<20.5C), thermal expansion is below 1.5 μm and is within the current placement alignment error.
- Above 20.5C to 22.2 C, the thermal expansion increases to 2.95 μm , significant enough to cause unwanted variations in chiplet print placement.
- Above 22.2C, the thermal expansion increases significantly and would be detrimental to large array printing.
- Although the variation of the internal temperature of the micro transfer printer is small, accurate temperature measurements and control must be made to ensure consistent printing over extended periods..
- These results need to be validated experimentally to compare the actual thermal expansion at each temperature point used in this study.
- Additives in the stamp and geometric designs may assist in heat dissipation, extending the working window of the PDMS stamp.

Thank You
creyes@X-Celeprint.com