

# Rotor modeling at low temperature for NMR

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**Introduction:** Two laboratories of CEA, SBT and SCIB, are developing a novel technique of NMR taking advantage of low temperature. A cold (down to 10K) rotating (up to 30 kHz) rotor allows for quicker and more precise spectrum.

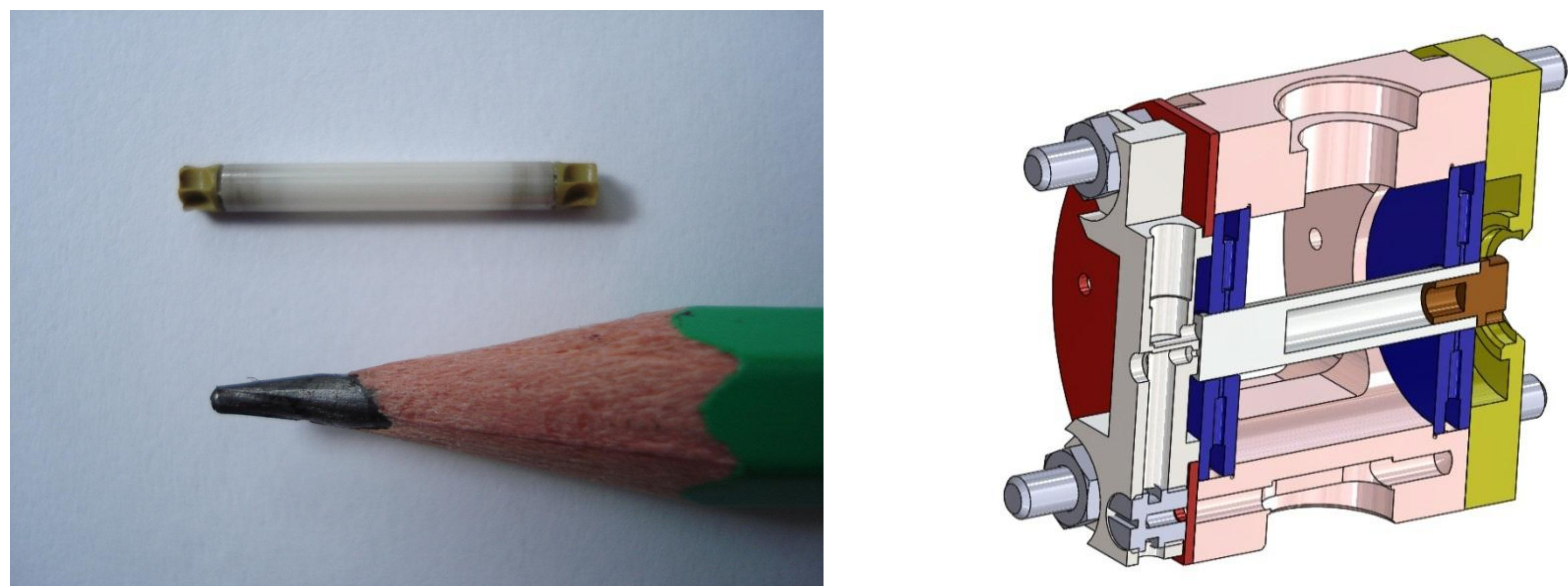


Figure 1. MNR rotor (left); a view of its chamber (right)

The rotor is maintained in its chamber by two aerostatic bearings (two Helium mass flow)

**Computational Methods:** two “Thin-Film Flow” interfaces have been used. The geometry is shown in figure 2, left.

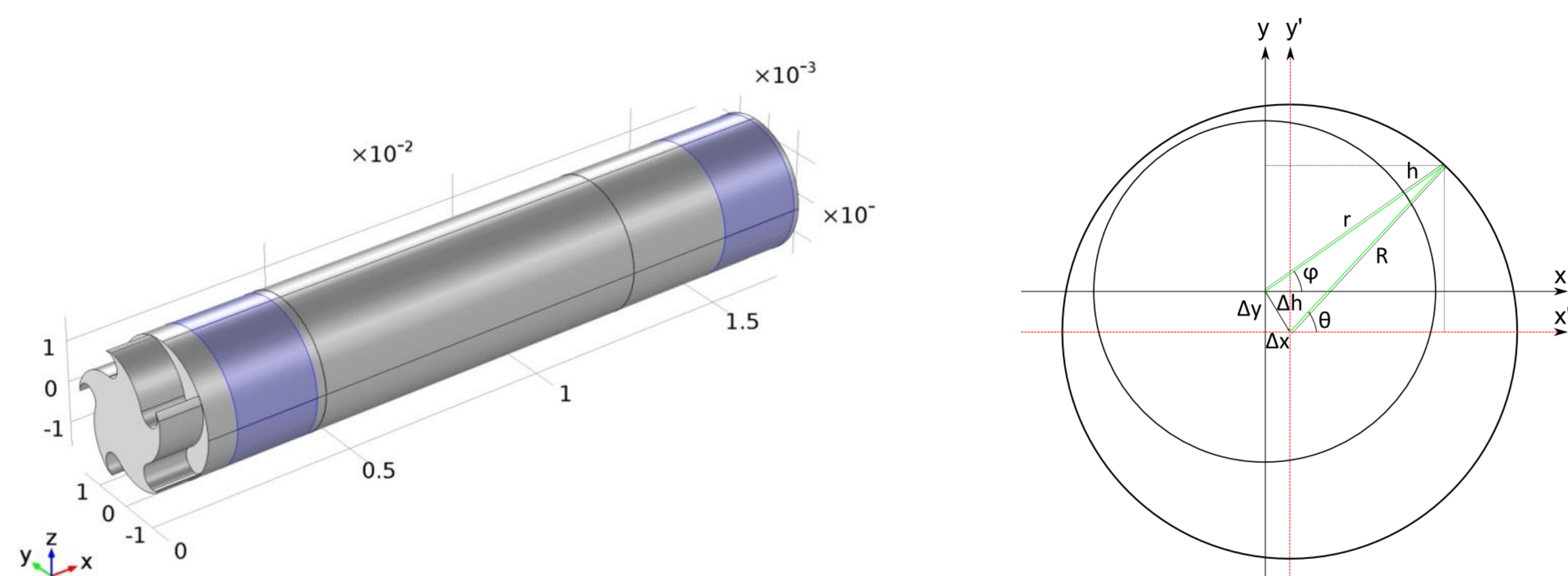


Figure 2. left : Modeled rotor. In blue, the aerostatic bearings. Right, the film thickness  $h$  and eccentricity

In addition, additional global equations has been use to calculate the film thickness (figure 2, right, eq.1) as

Well as the interaction between the two bearings (eq.2).

$$\begin{cases} \iint F_{x_{fl \rightarrow p}} \cdot dS = m \cdot \ddot{\Delta}x \\ \iint F_{y_{fl \rightarrow p}} \cdot dS = m \cdot \ddot{\Delta}y \end{cases}$$

$$\begin{cases} \frac{m}{2} \ddot{x}_b + \frac{m}{2} \ddot{x}_f + \iint F_{b_x_{fl \rightarrow p}} \cdot dS + \iint F_{f_x_{fl \rightarrow p}} \cdot dS = 0 \\ -\frac{I}{2 \cdot L^2} \ddot{x}_b - \frac{I}{2 \cdot L^2} \ddot{x}_f - \iint F_{b_x_{fl \rightarrow p}} \cdot dS + \iint F_{f_x_{fl \rightarrow p}} \cdot dS = 0 \\ \frac{m}{2} \ddot{y}_b + \frac{m}{2} \ddot{y}_f + \iint F_{b_y_{fl \rightarrow p}} \cdot dS + \iint F_{f_y_{fl \rightarrow p}} \cdot dS = 0 \\ -\frac{I}{2 \cdot L^2} \ddot{y}_b - \frac{I}{2 \cdot L^2} \ddot{y}_f - \iint F_{b_y_{fl \rightarrow p}} \cdot dS + \iint F_{f_y_{fl \rightarrow p}} \cdot dS = 0 \end{cases}$$

As the rotor is rotating, the resulting couette flow creates a parietal pressure and the precession of the rotor (fig. 3).

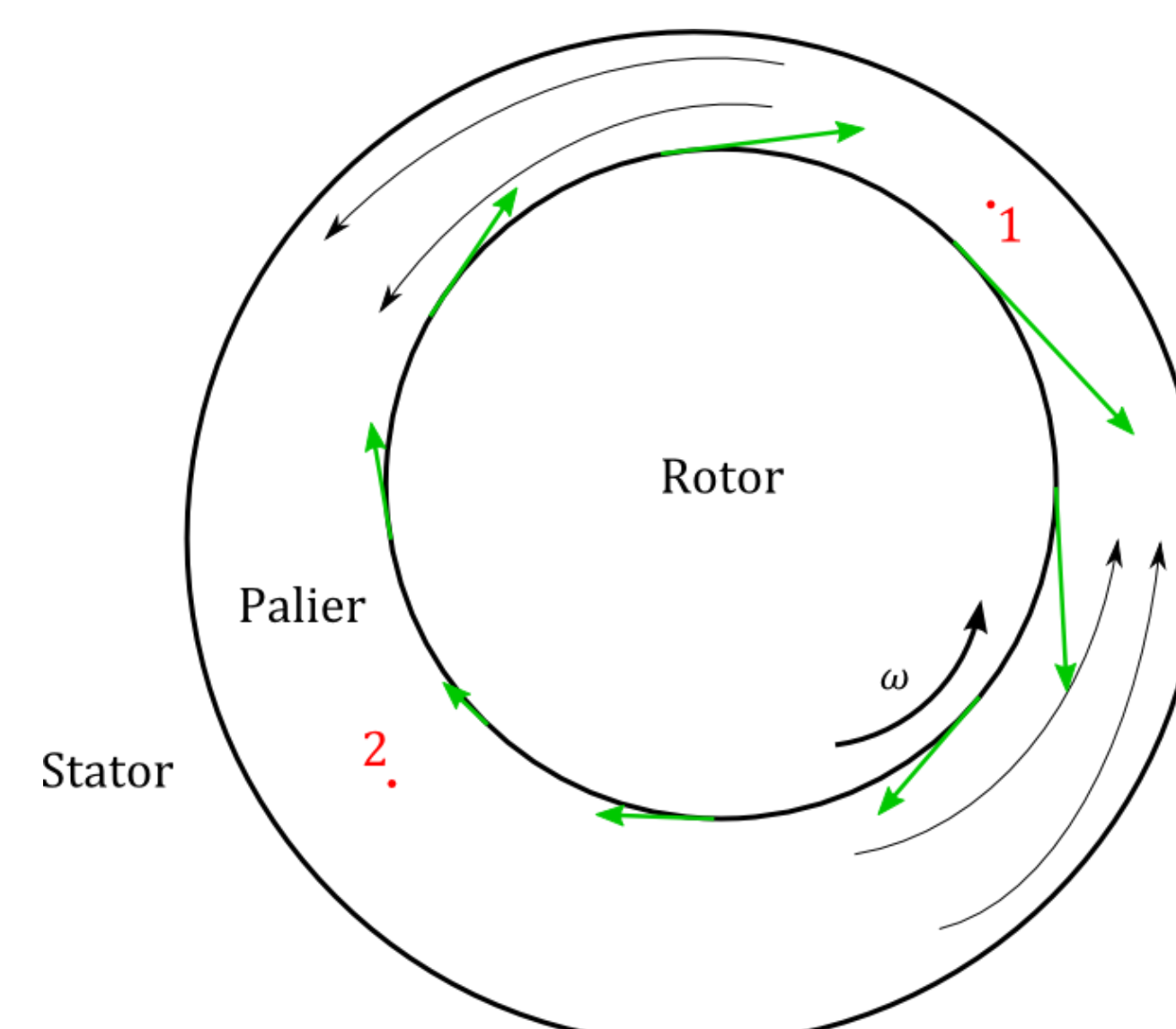


Figure 3. Couette flow and the parietal pressure (green)

**Results:** Both direct and cross bearings rigidities have been calculated as a function of the Helium mass flow. The results shows an optimum in the mass flow (figure 4).

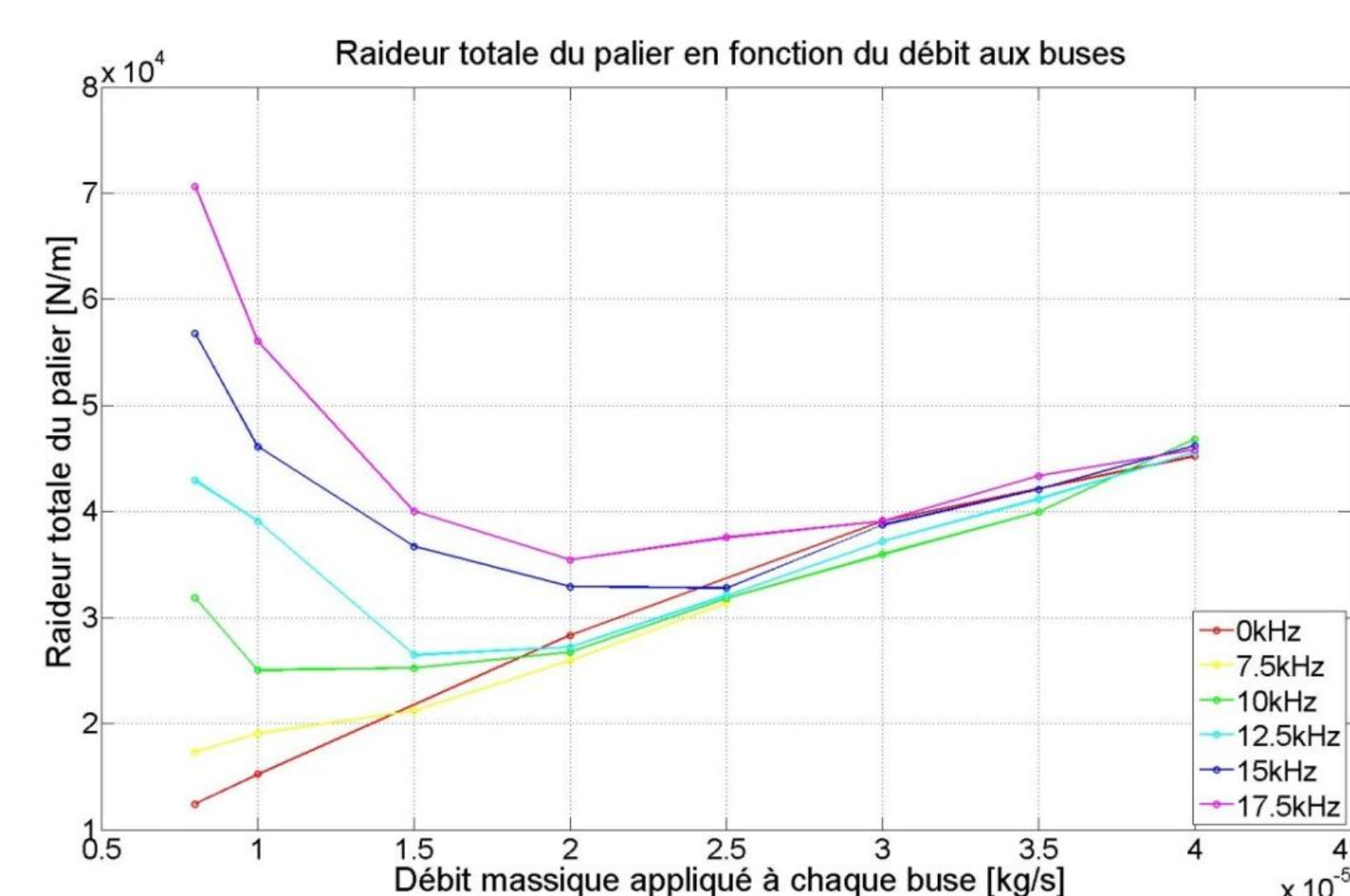


Figure 4. Bearings rigidity as a function of the Helium mass flow for different rotation frequencies

The precession radius as a function of the mass flow has also been calculated. It shows a mass flow optimum.

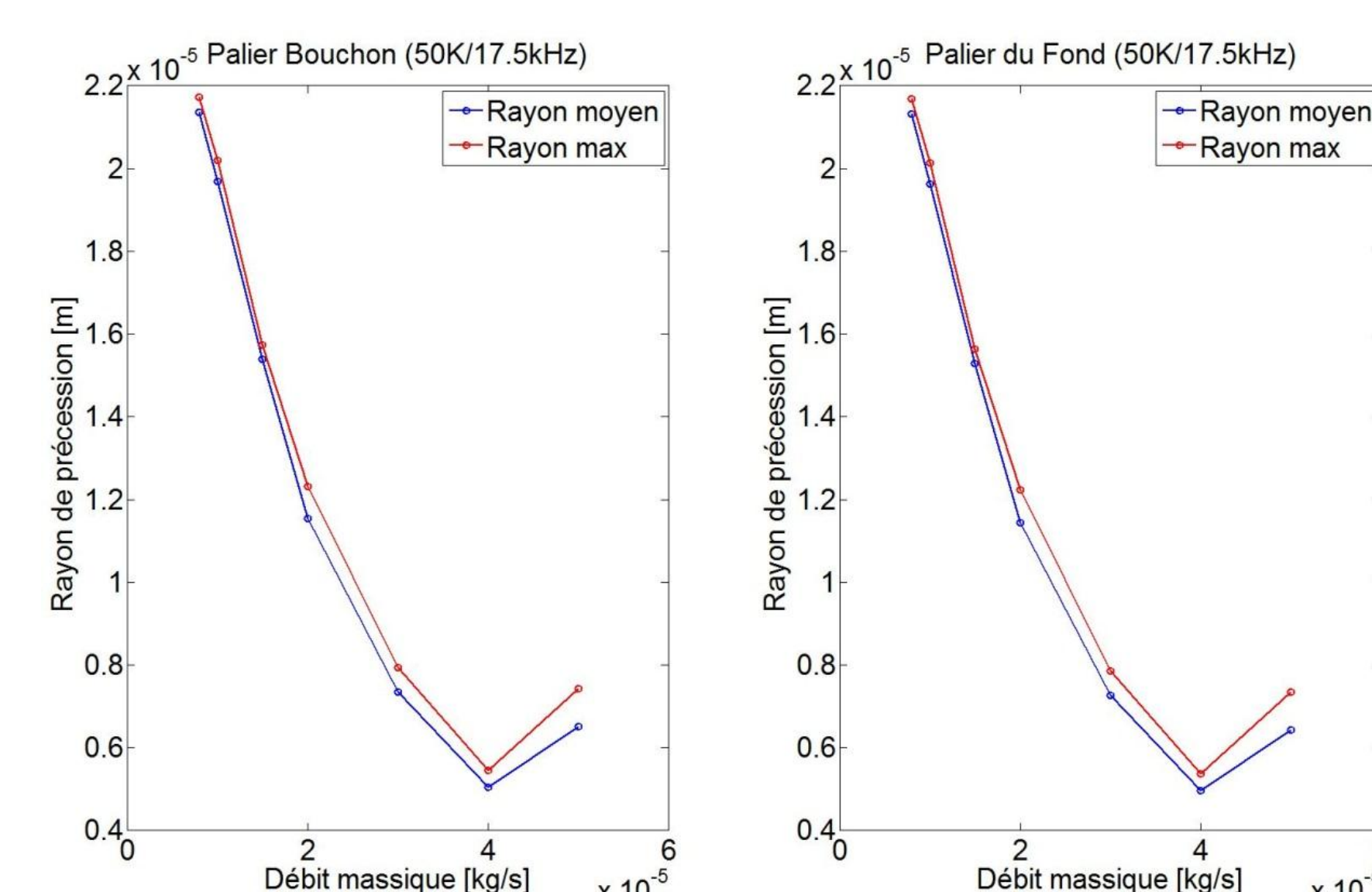


Figure 5. Precession radius as a function of rotor rotation frequency at different mass flow

**Further developments:**

- \* Viscous dissipation heating: taking into account the temperature variation
- \* Rotor rotation : study of the fluid/structure interaction of the rotation creation by an additional helium flow.