

DE LA RECHERCHE À L'INDUSTRIE



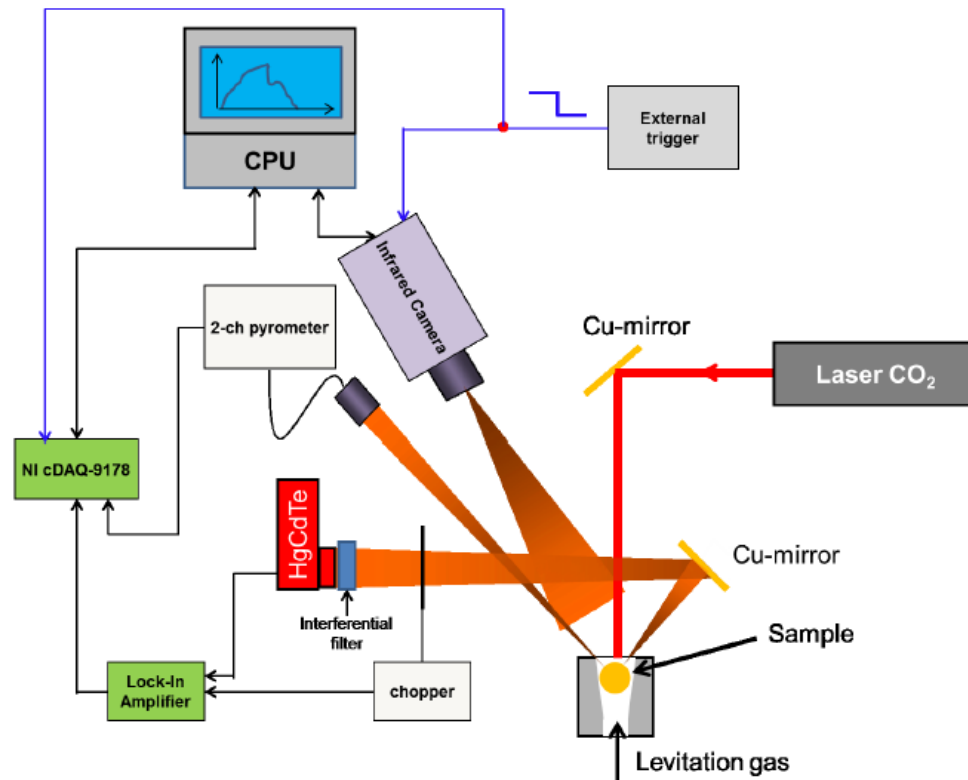
# Simulation of an aerodynamic furnace for high temperature data acquisition using Comsol® Multiphysics

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## LEVITATION METHODS

Method	samples	heating	Typical size (mm)	Main limitations
Acoustic	Any	Laser	0,5-3	Limited temperature
Aerodynamic	Any	Laser	0,7-3	Gas footprint ?
Electrostatic	Any	Laser	1-4	Require stable electrical charge on sample
Electromagnetic	Conductor	RF/laser	2-10	conductors
Optical	Non reflective	Laser	0,0001	Very small samples
Gas film	Any	Radiative	Up to 30	Limited temperature



## Advanced Temperature and Thermodynamic Investigation by Laser Heating Approach

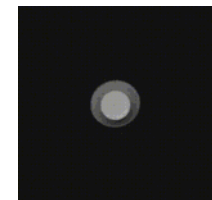
Spherical sample heated by laser up to 3200 K.

**Pyrometer** for temperature

**Infrared Camera** for position and volume

Oscillations :

- **Surface Tension**
- **Viscosity**

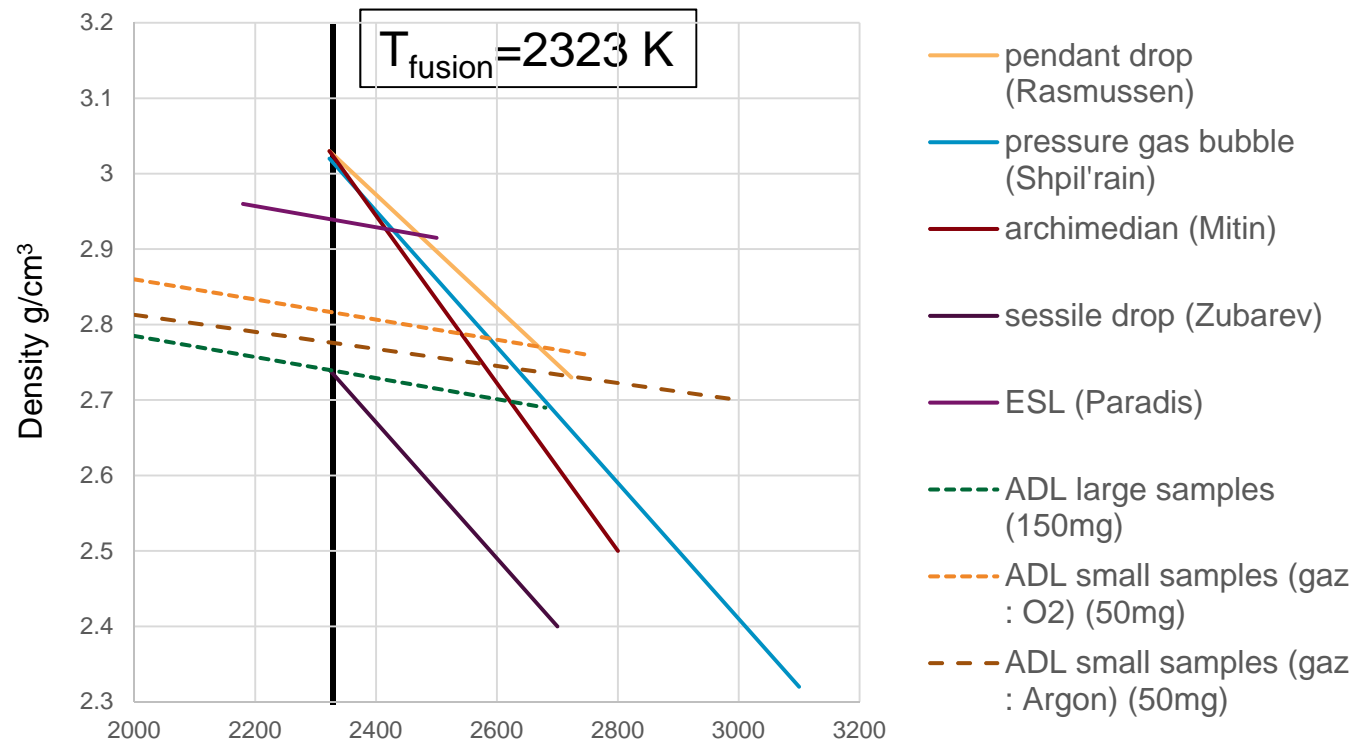


- Laser cut off :

- **Density as function of temperature**
- **Specific Heat Capacity**

Aerodynamic levitation : access to undercooled liquids – very large temperature range

# EVALUATION OF LIQUID ALUMINA DENSITY AS A FUNCTION OF TEMPERATURE –QUICK REVIEW

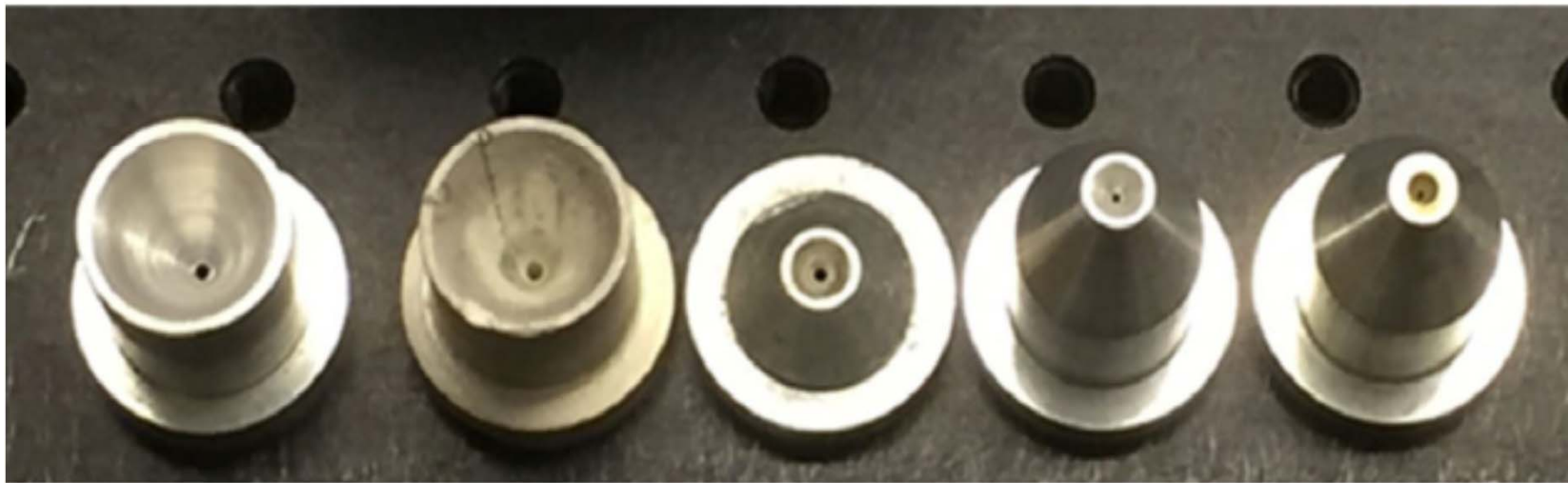


Apparent **Chemical contamination** for container based technics (pendant drop, archimedian, pressure bubble)

Similar **trends** for containerless (levitation) technics (ESL and ADL)

But **ADL** give **lower values** at fusion point, dependent of sample size and levitation gas type !

# SIDE VIEW OF MOLTEN OXIDES LEVITATION AND TYPICAL NOZZLES\*



Density currently evaluated assuming **spherical shape**

\* : C.J. Benmore and Weber aerodynamic levitation ,supercooled liquid and glass formation, advances in physics X, 2:3 737-736.

## QUESTION :

Is the liquid levitated sample really spheric ?

Lets have a look using ....

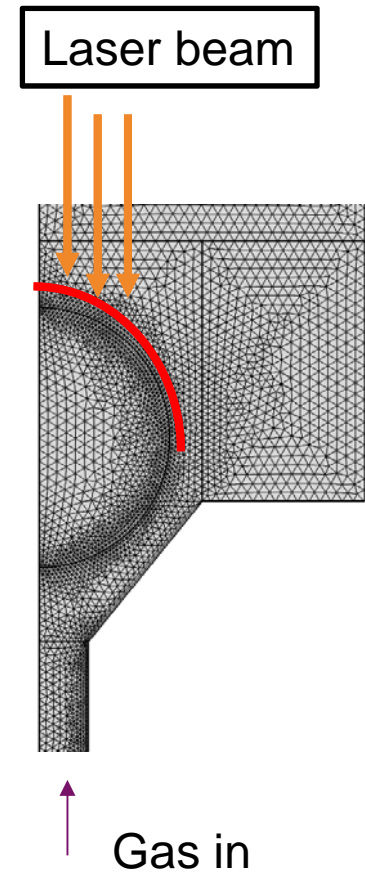
**Comsol® Multiphysics**

Challenges :

- Temperature gradient (**1000 K / 10  $\mu\text{m}$** ) close to LG interface
- Sample position in nozzle: major impact on gas flow
- Strong Marangoni effect due to temperature gradient (200K) inside sample before laser cut-off

Software :

**Heat + Microfluidic Comsol® modules + moving mesh ALE**  
(first order Winslow smoothing for LG interface temporal evolution)



## Convergence strategy :

Preliminary thermomechanical solution :  
**Undeformable** spherical sample – **no gravity** – **ramping** viscosity

Controlled temporal iteration until stationary solution :

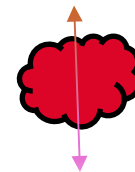
### Balance internal and external forces at LG interface

$$\delta T = 1 \text{ e-}08 \text{ s} \quad \Delta T = 1.\text{e-}04 \text{ s}$$



### Vertical stabilization of sample

$$\delta T = 1 \text{ e-}05 \text{ s} \quad \Delta T = 1.\text{e-}02 \text{ s}$$



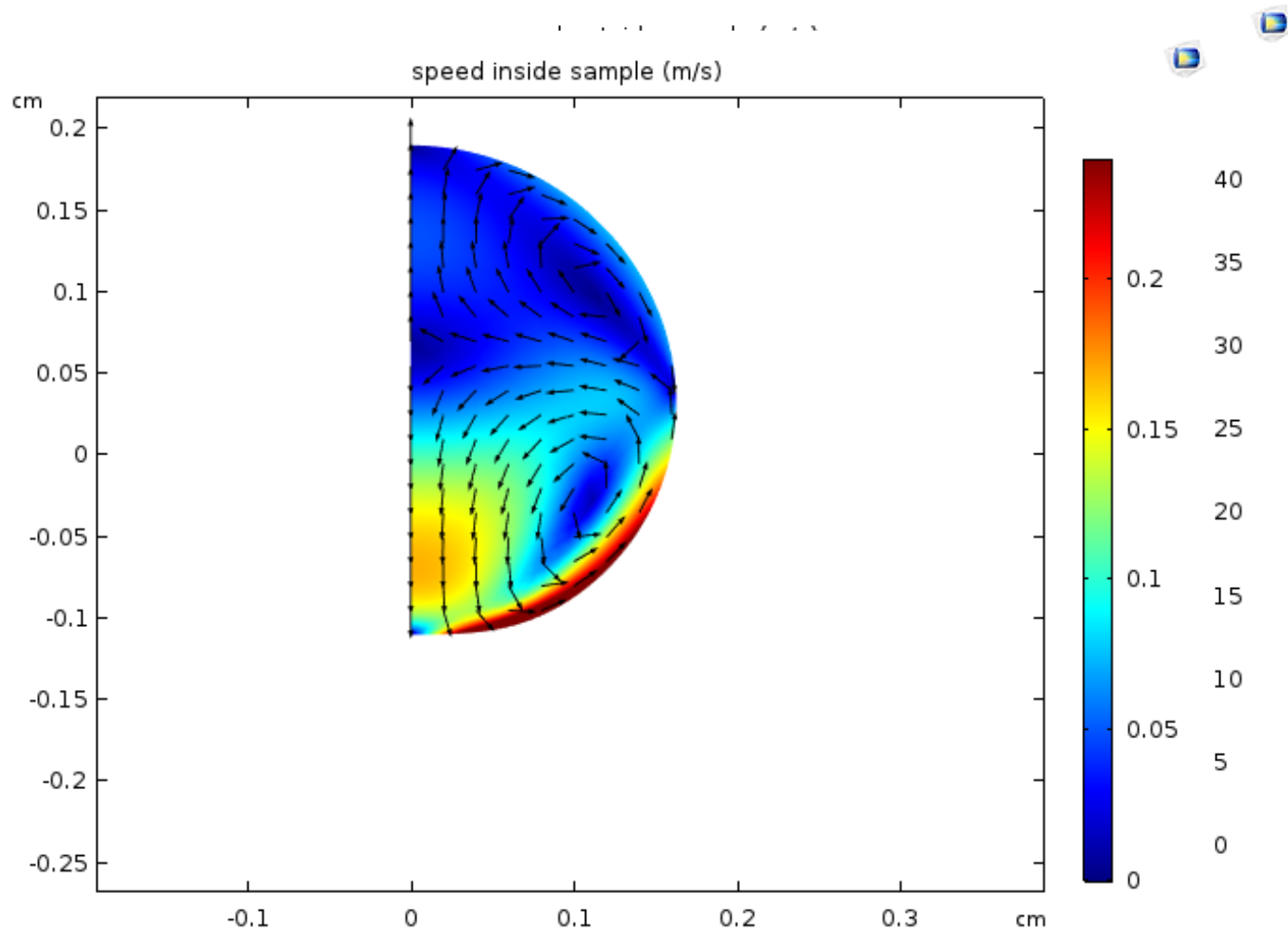
### Convergence of internal liquid flow

$$\delta T = 0,001 \text{ s} \quad \Delta T = 2 \text{ s}$$

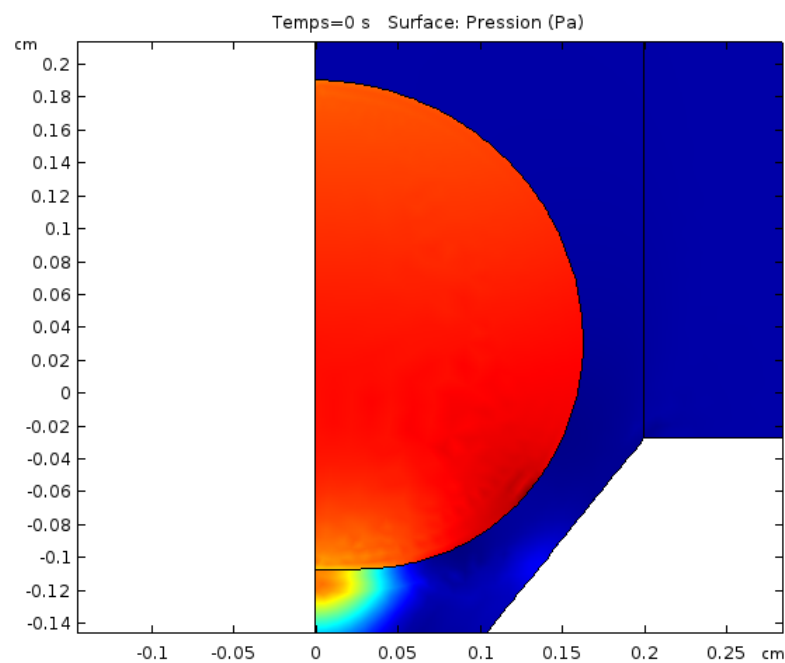




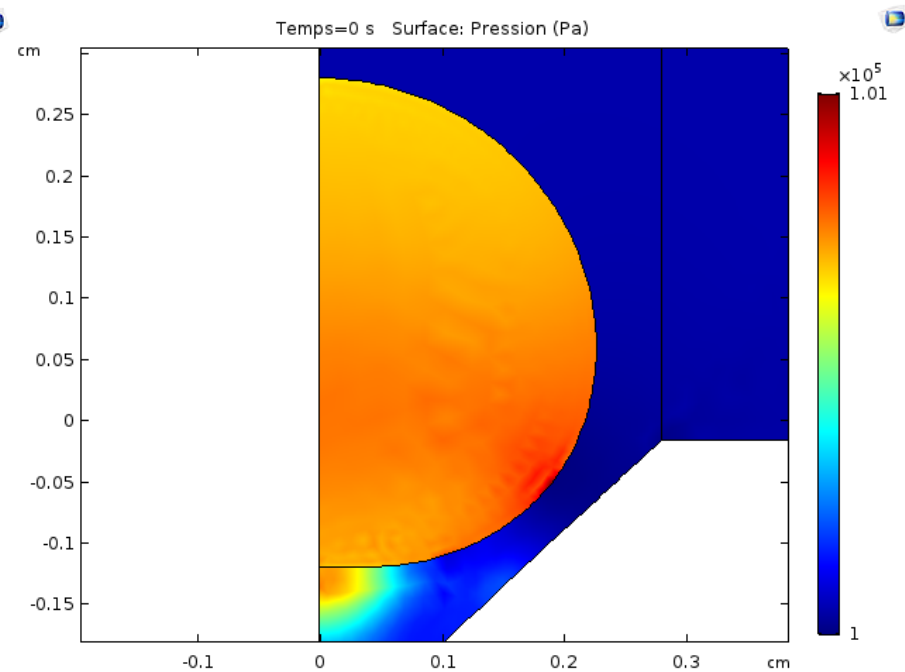
# FLUID VELOCITY RESULTS



# IS THE SAMPLE SPHERICAL ? COMSOL ANSWER:



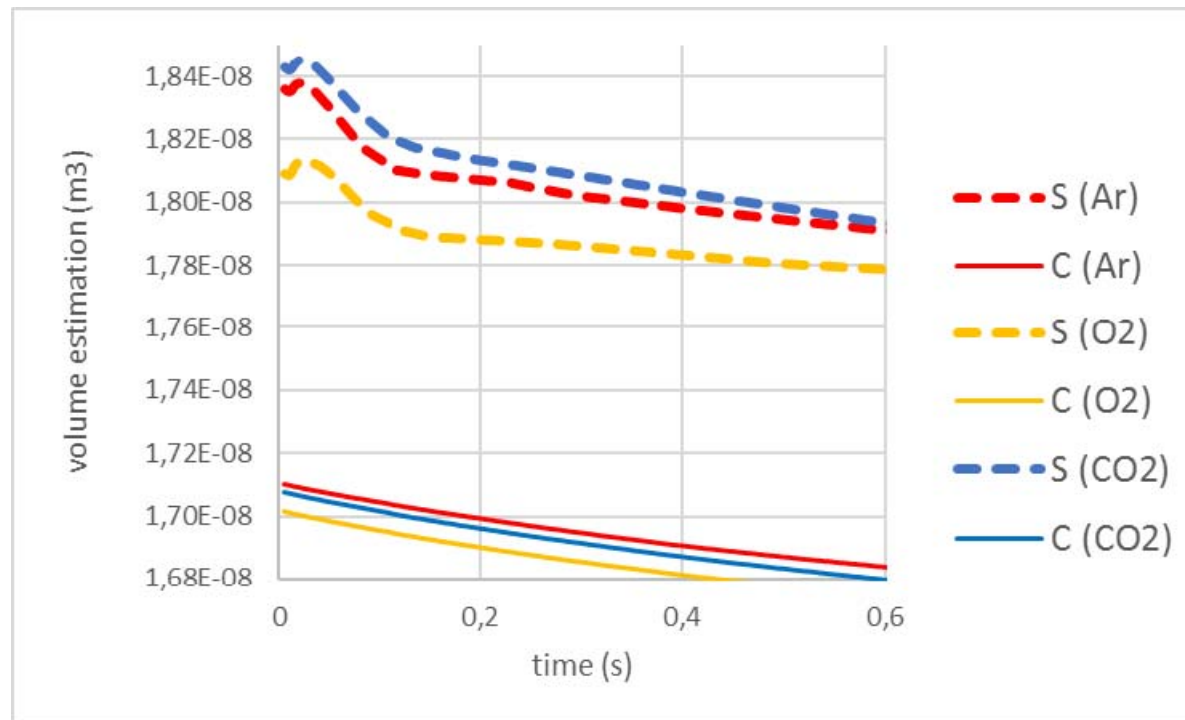
50 mg alumina



130 mg alumina

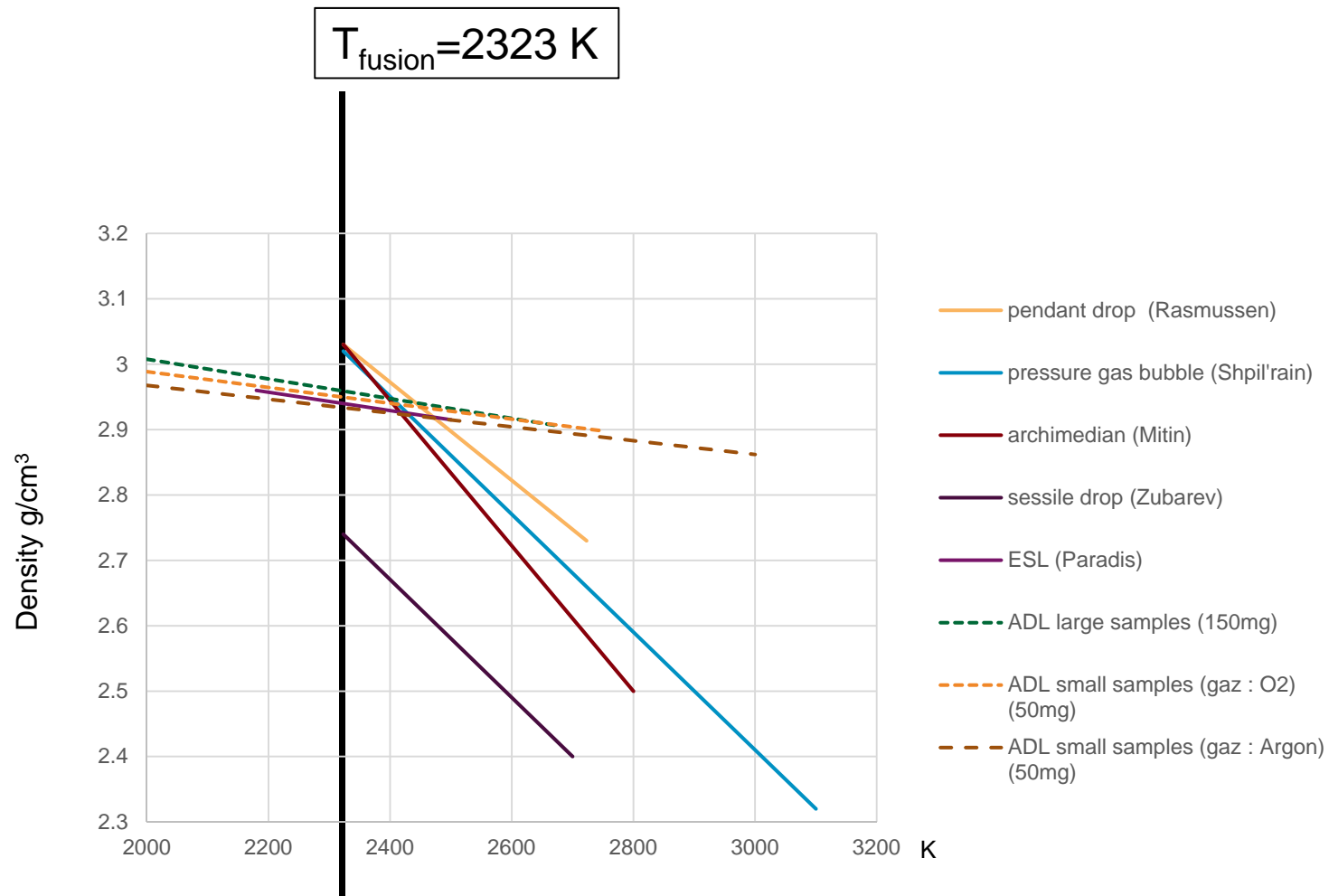
The **TOP** of the sample remains **spherical**  
The **BOTTOM** get more and more deformed as its size increases

# VOLUME ESTIMATION AFTER LASER CUT-OFF FOR VARIOUS LEVITATION GAS



S : assuming spherical approximation  
C : volume calculated by Comsol

# DENSITY ESTIMATION WITH CORRECTED VOLUME



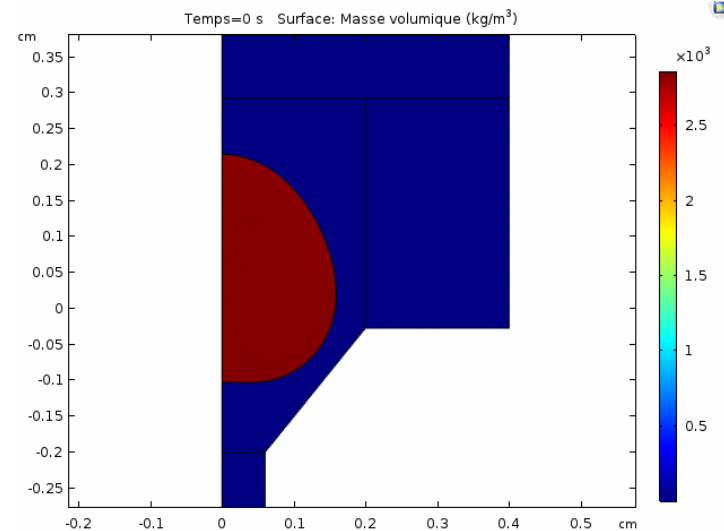
Levitation technics give now similar results.  
Difference at fusion probably due to recalescence of the sample

## CONCLUSION :

Using Comsol® multiphysics it seems possible to adjust the **density evaluation** of aerodynamic levitation

On going work on other thermodynamical data :

- **heat capacity**
- **viscosity**
- **surface tension**



**Thank you for your attention !**

**Questions and comments  
are welcome !**

# CURRENT HEAT CAPACITY AND TEMPERATURE EVALUATION HYPOTHESIS

**Main hypothesis** (similar to other levitation technics) **only radiative decay after laser cut-off:**

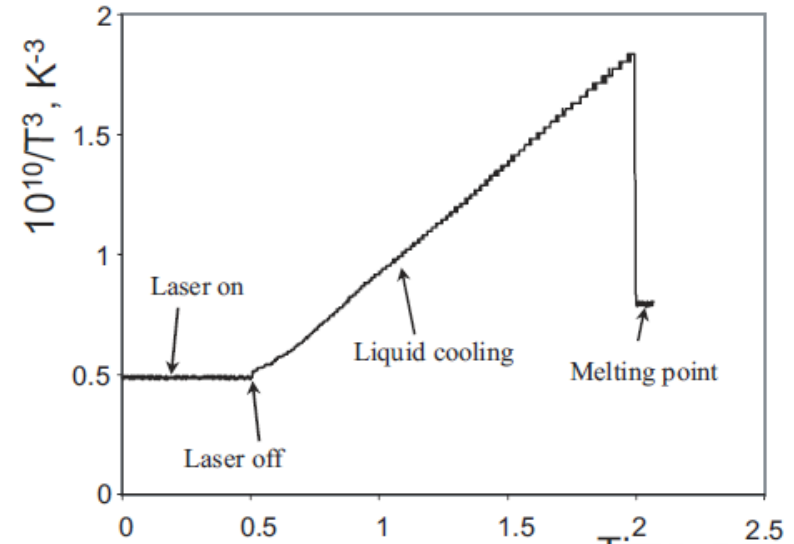
$$\frac{dQ_R}{dt} = \varepsilon k_B S (T^4 - T_0^4) \cong \varepsilon k_B S T^4 \quad (1)$$

Energy balance on sample

$$m C_p dT + dQ_R = 0 \quad (2)$$

$$\frac{dT}{dt} = - \frac{\varepsilon k_B S T^4}{m C_p}$$

$$\frac{C_p}{\varepsilon} = - \frac{k_B S d(\frac{1}{T^3})/dt}{m}$$



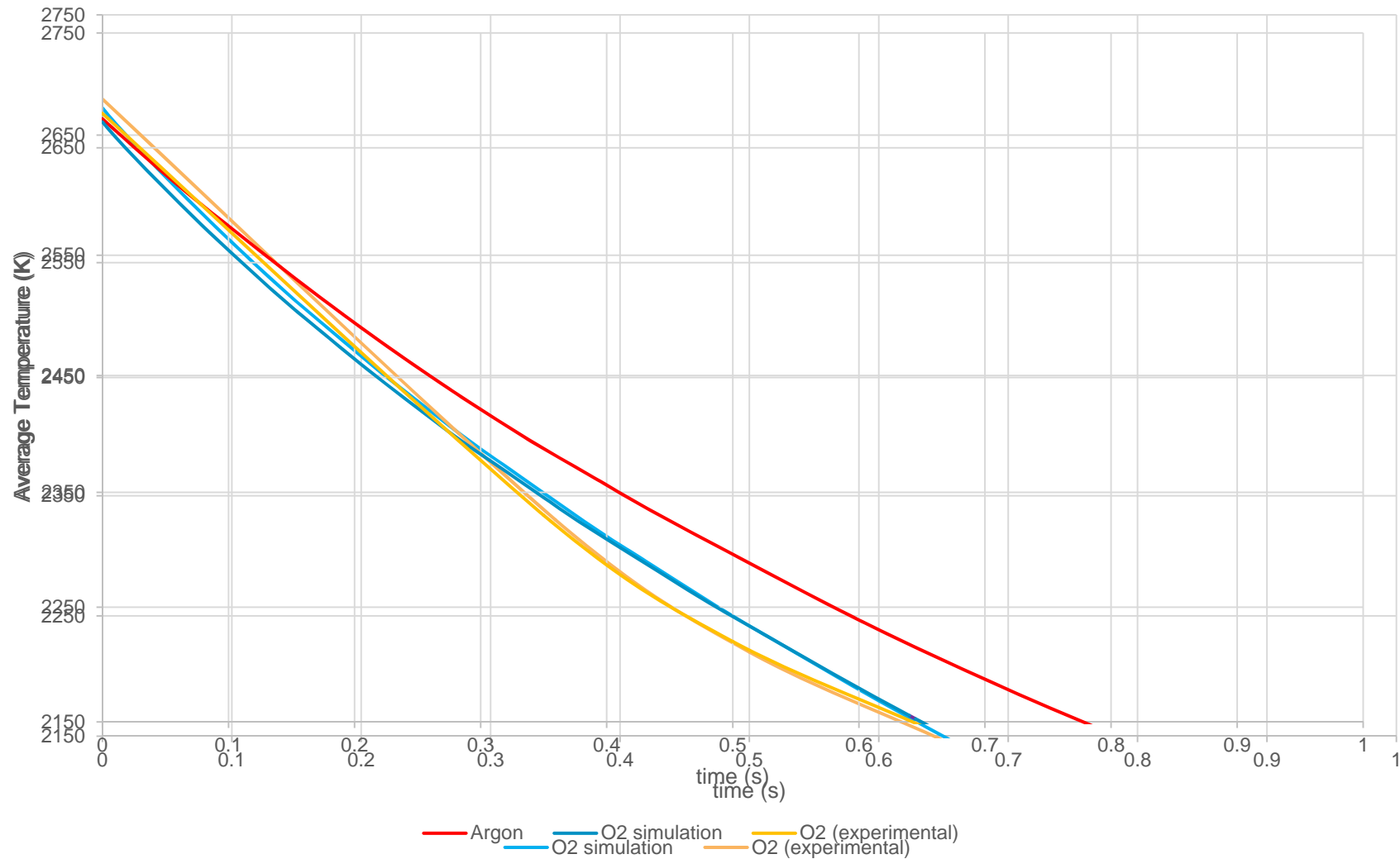
Apparently true but not proven ...

- $Q_R$  radiative heat
- $t$  time
- $\varepsilon$  hemispherical total emissivity
- $k_B$  Stefan Boltzmann constant
- $S$  surface
- $T$  sample temperature
- $T_0$  ambient temperature
- $m$  sample mass
- $C_p$  specific heat capacity





# INFLUENCE OF LEVITATION GAS ON TEMPERATURE DECAY



Decay is not purely radiative and depends on gas conductivity

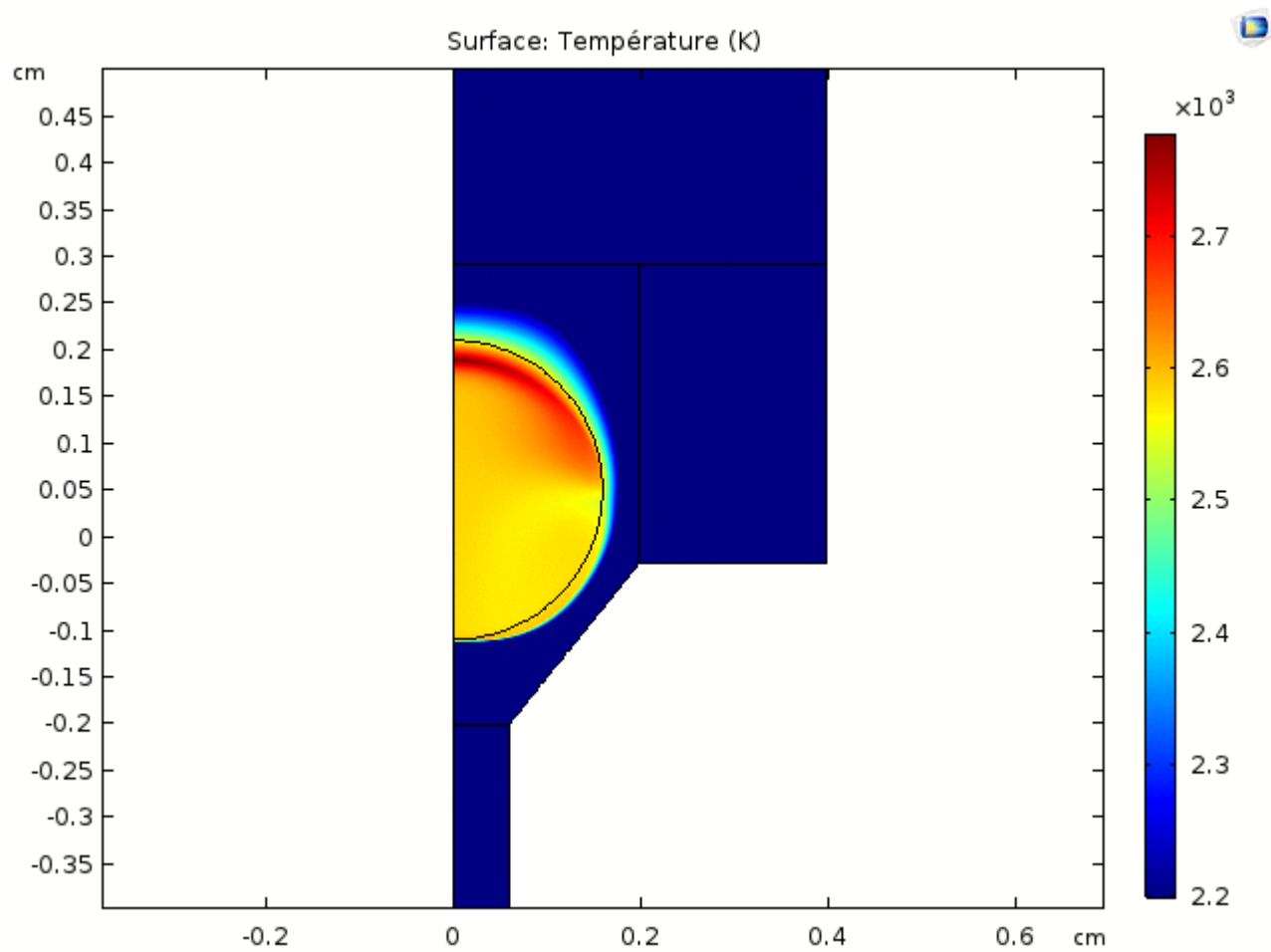
# THERMODYNAMIC DATA AT DIFFERENT TEMPERATURES

T=300 K	Air	Xenon	Oxygen	Argon	Helium
Conductivity (W/mK)	0,026	0,0055	0,026	0,018	0,152
Viscosity (10 <sup>-5</sup> Pas)	1,82	2,2	1,95	2,1	0,88

T=3000 K	Air	Oxygen	Argon
Conductivity (W/mK) (e)	0,383	0,802	0,09
Viscosity (10 <sup>-5</sup> Pas) (e)	8,58	9,49	10

Hypothesis : air /oxygen at thermal equilibrium

# TEMPERATURE EVOLUTION AFTER LASER CUT-OFF



Temperature get homogenised in a few ms